

Use of Mass Discharge as a Performance Metric in CERCLA Decision Documents

Case Study of the Time Oil Well 12A Site

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**CDM
Smith**

Acknowledgments

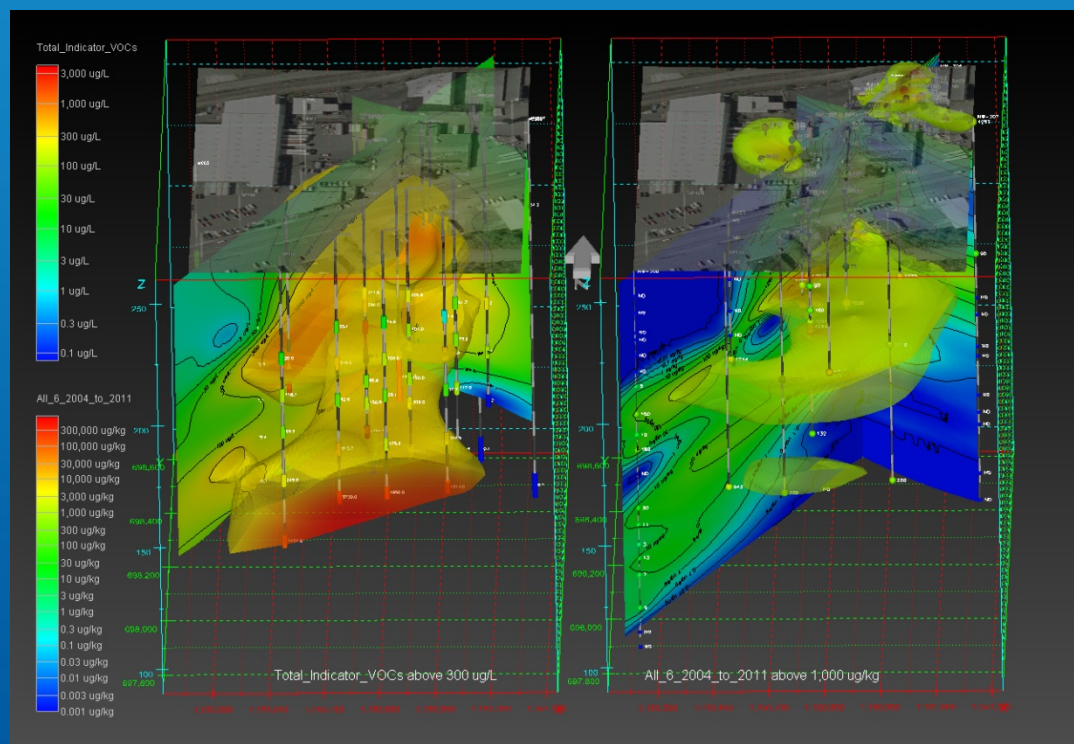
- Kira Lynch
- Howard Orleans (EPA Region 10)
- Tamzen Macbeth (CDM Smith)

Presentation Context

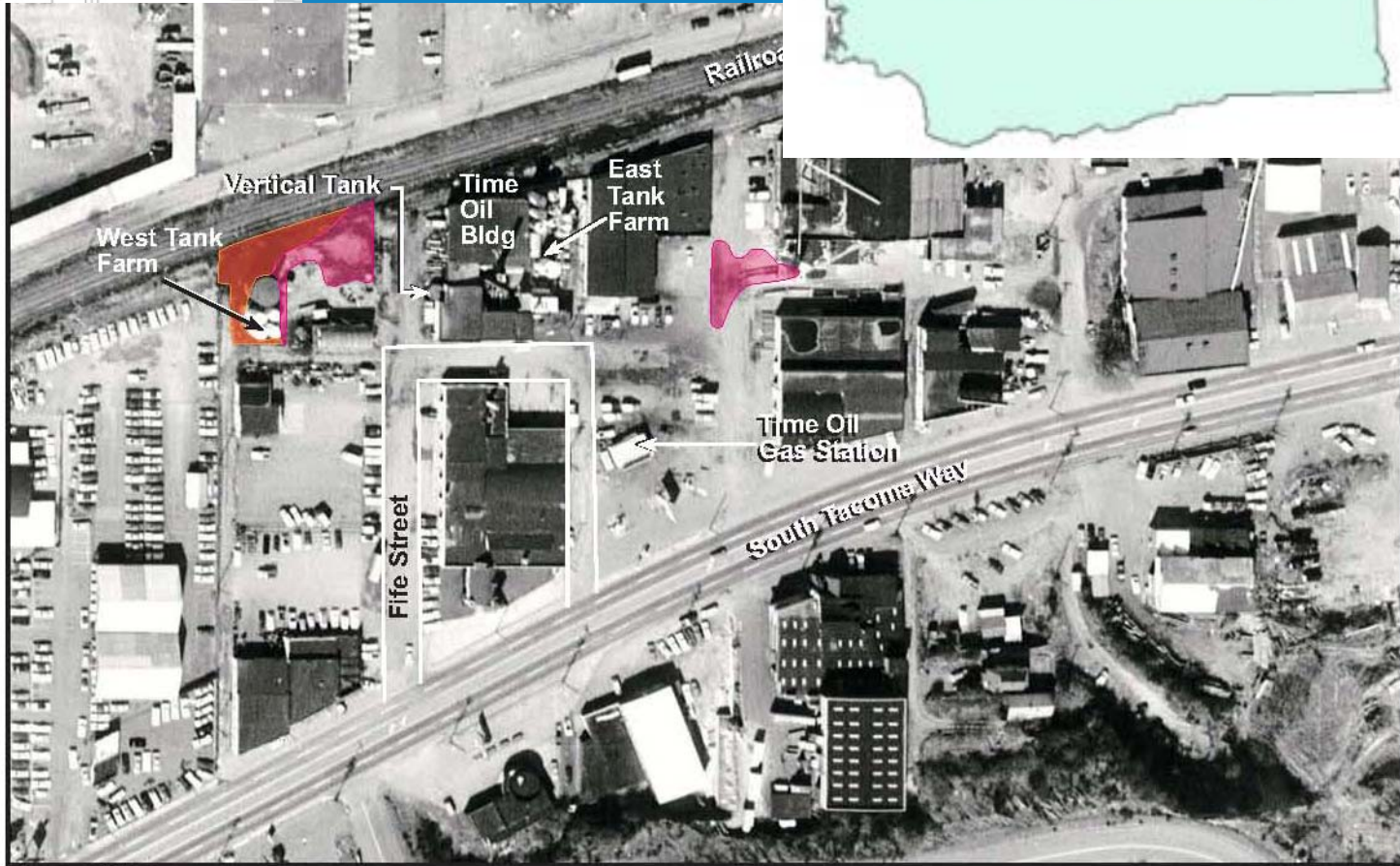
- Many CERCLA decision documents for dense non-aqueous phase liquid (DNAPL) site remediation lack clear remedial action objectives for determining and documenting when sufficient source treatment has been completed.
- Mass flux /discharge can be used to document when source treatment is considered “complete” and long-term groundwater restoration projects considered operational and functional.
- Discuss how mass flux /discharge goals can be incorporated into long-term plume management strategies with ultimate goals of meeting Maximum Contaminant Levels (MCLs).

Well 12a Case Study: Applying Mass Flux/Mass Discharge

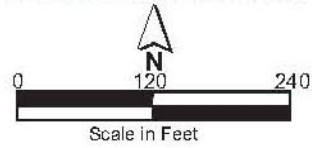
- Well 12A is a case study for how to evaluate a Remedy treatment of dense non-aqueous phase liquid (DNAPL) source.
- Discuss the process of how mass flux/discharge was incorporated into:
 - Record of Decision (ROD).
 - Technology Selection,
 - Remedy Design,
 - Optimization of the Remedy



Site Location



Parametrix EPA 415-23228-007/014A(F102) 3/08 (B)/h



- Disturbed / stained soil
- Heavily stained soil

Figure
Aerial Photograph of
Time Oil Site (1969)

Contamination Summary

- Six COCs in soil and groundwater
 - PCE
 - TCE (ubiquitous)
 - cis-1,2 DCE
 - trans-1,2 DCE
 - Vinyl Chloride
 - 1,1,2,2-PCA

2D Perspective: TCE Plume



Historical RA Summary

- 1983- Original signed ROD
 - Wellhead treatment system at Well12A
- Groundwater Extraction Treatment System (GETS)
 - 1988 – 2001
 - 550 million gallons of groundwater extracted/treated,
 - removed 16,000 pounds VOCs
- Vapor Extraction System (VES)
 - 1993 – 1997/Removed 54,100 pounds VOCs
- Filter cake/contaminated soil removal
 - BNRR excavated 1,200 cy along rail line
 - VES construction/removed 5,000 cy of filter cake

Desired End State

- Adequate use of robust source removal technologies.
- Timely transition to cost-effective ‘polishing’ step(s).
- Reduce/eliminate need for pump and treat.
- Appropriate reliance on monitored natural attenuation (MNA).
- Adaptive, flexible implementation
 - *“Sources begin to reveal themselves as remediation progresses”*

Building the Well 12A Remedy

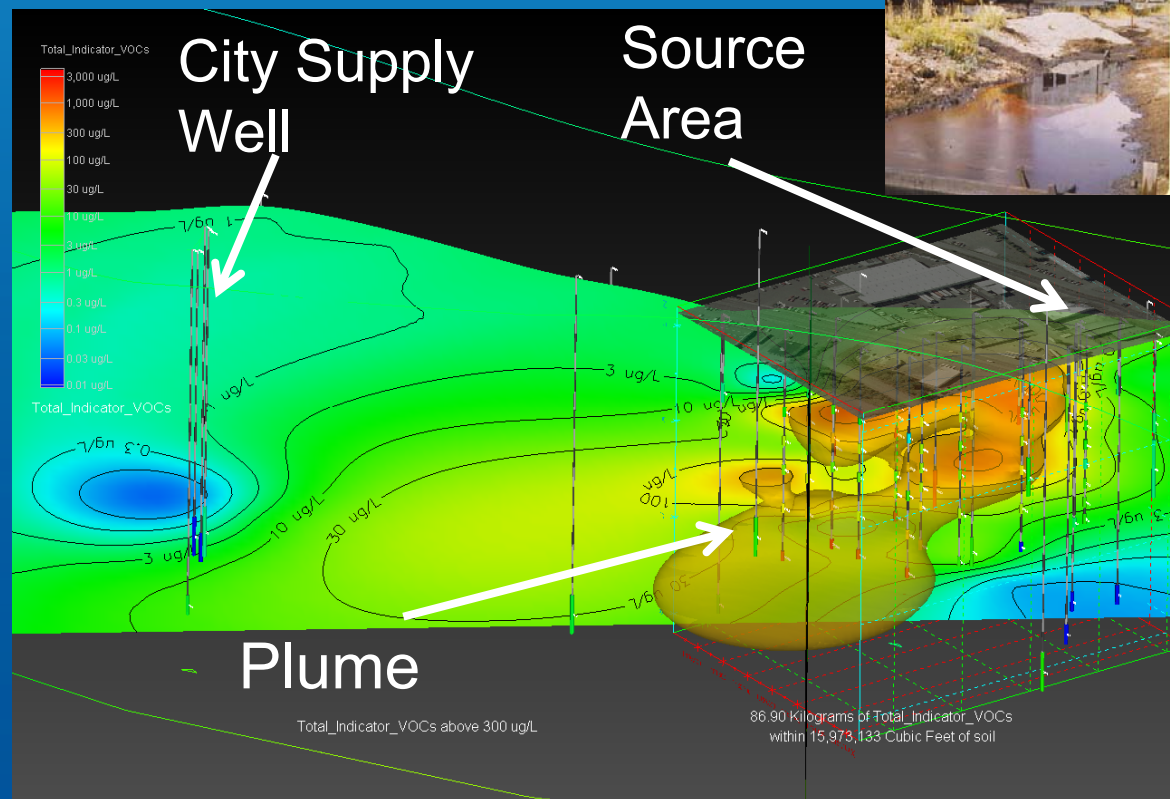
Focused Feasibility Study evaluation:

Reduce source strength (Md) by 90%, MNA sufficient to achieve **compliance**

ROD amendment:

Multi-component remedy- reduce source discharge Md by 90% & transition technology (if necessary)

- Well 12A Superfund Site, WA
 - Performance metric → remedy Operational and Functional





Summary of Site Characterization

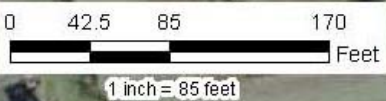


- 34 soil borings to reduce uncertainty and delineate sources.
- 12 locations for vertical profiling.
- Depth discrete samples:
 - Groundwater
 - Soil
 - Slug testing.
 - Stratigraphy
- Gradient assessment.

Legend

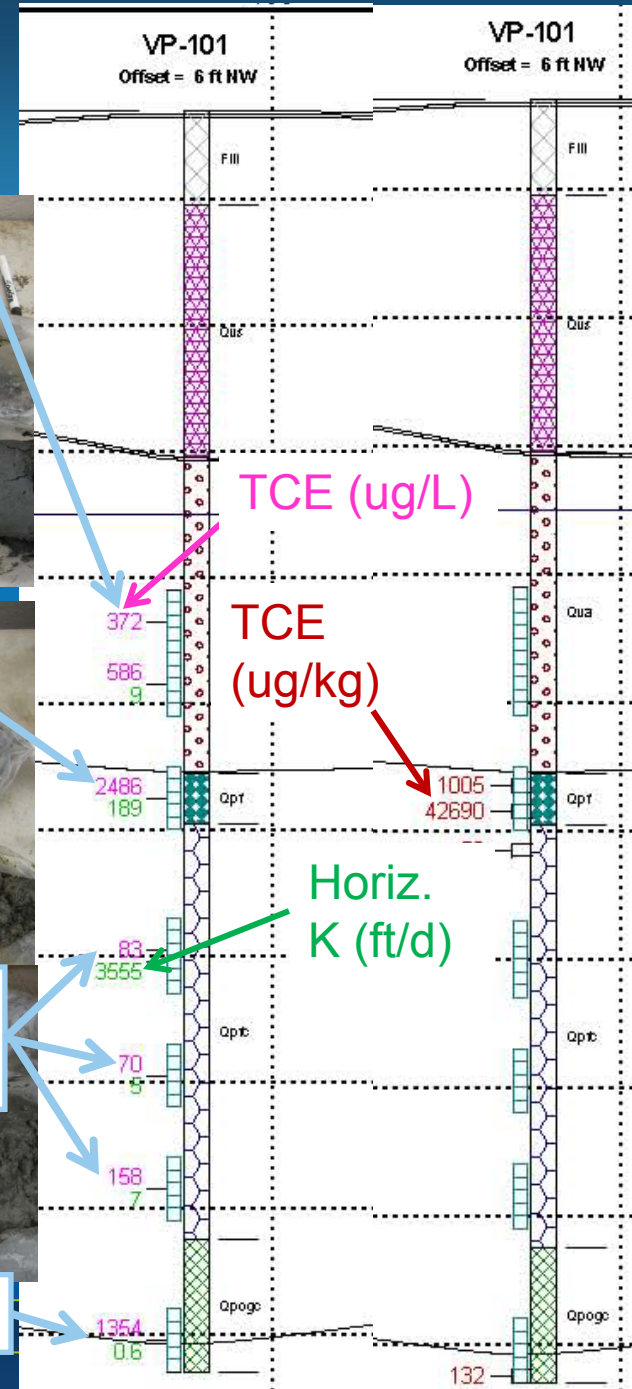
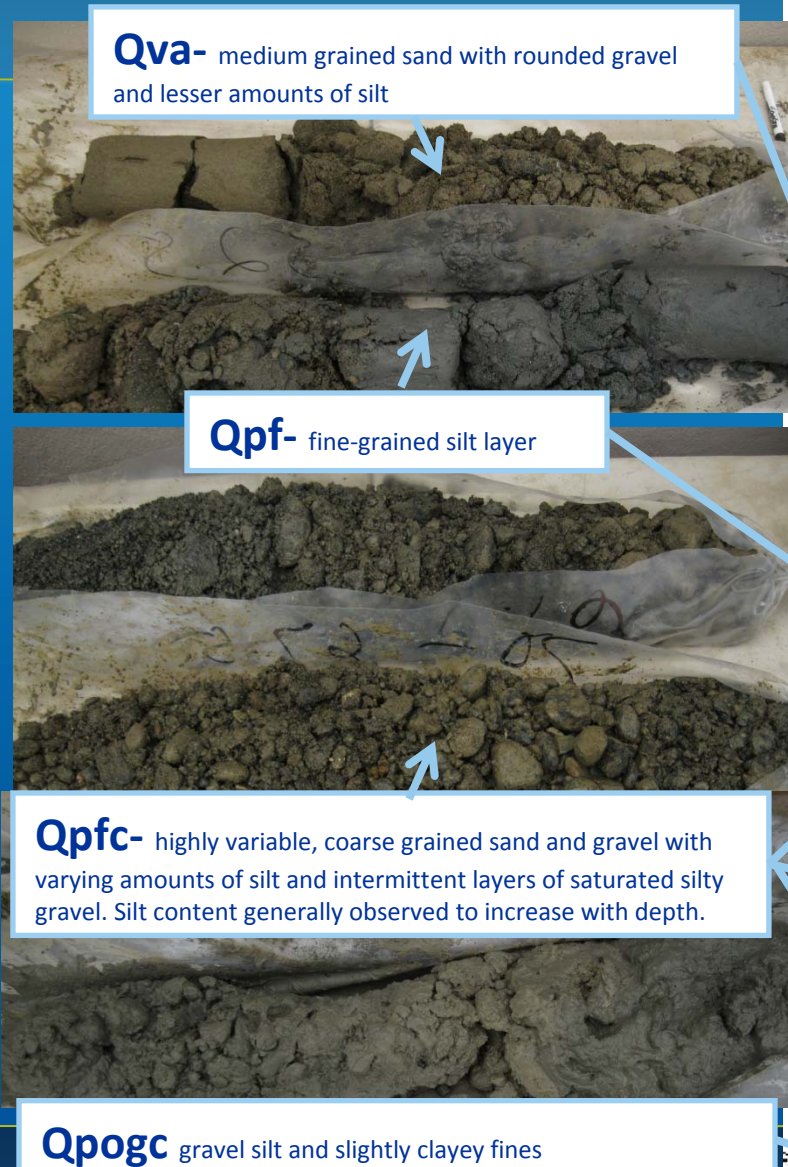
- Vertical Profile Location
- 2011 RDI Boring
- 2010 RDI Boring
- ⊕ Groundwater Monitoring Well

Acronyms:
 B - boring
 MW - monitoring well
 N - north
 RDI - Remedial Design Investigation
 VP - vertical profile



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Vertical Characterization



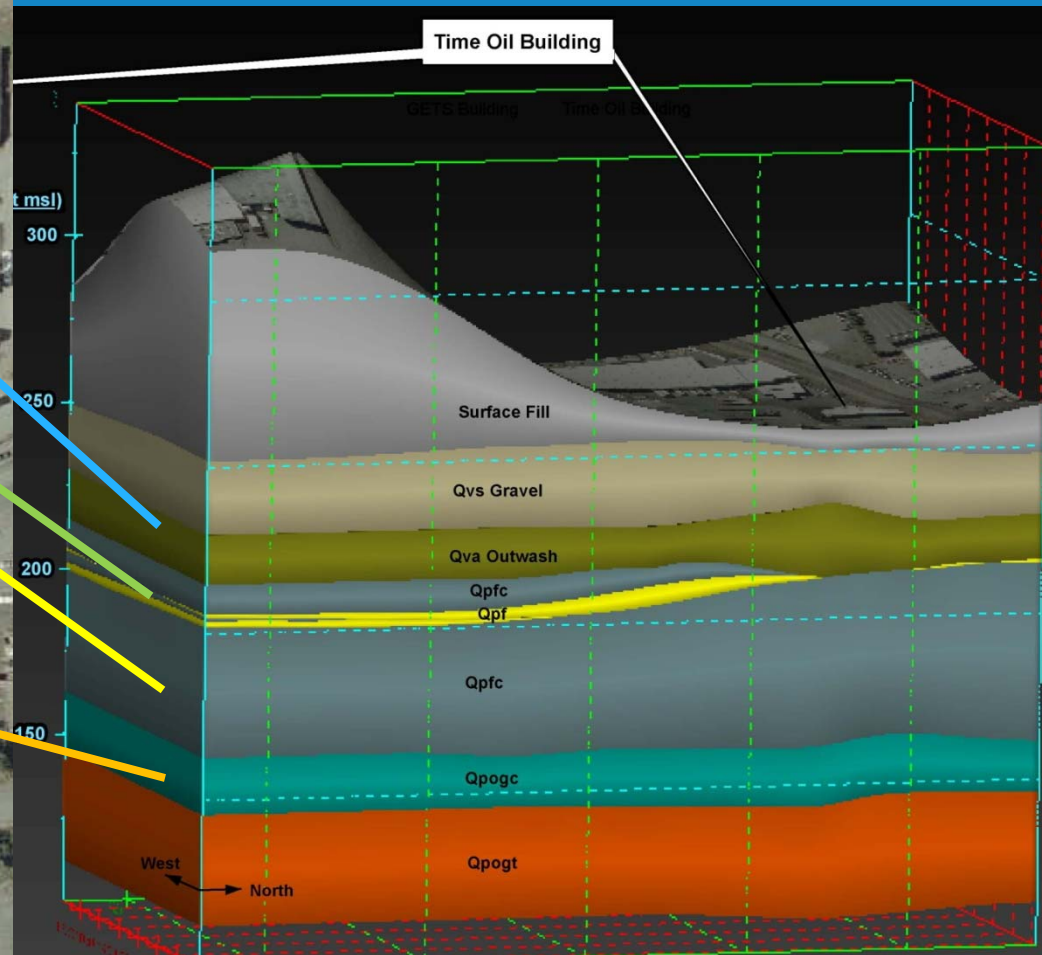
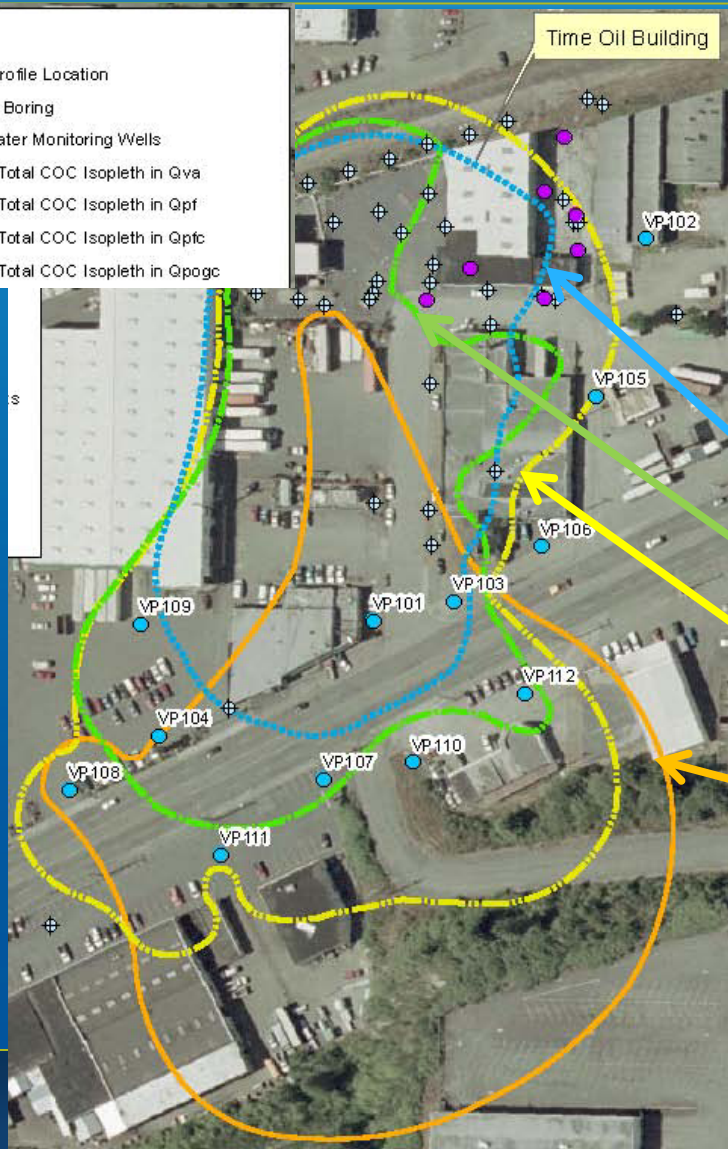
Hydraulic Conductivity: Slug Testing

Stratigraphic Unit	Range Horizontal K (ft/d)	Average Horizontal K (ft/d)	Vertical K (ft/d) ^a
Average K per Stratigraphic Unit Used in MVS			
Qva	7-56 (n=4)	21	5.18
Qpf	0.12-0.5 (n=2)	0.3	NA
Qpfc	0.5-3555 (n=14)	293	0.79
Qpogc	0.6-2 (n=5)	1	0.30
Qpogt	0.5 (n=1)	0.5	0.03
Average K per Depth Measured in Qpfc			
	Depth Interval (ft bgs)	Number Samples	Horizontal K (ft/d)
Qpfc1	50-60	5	35
Qpfc2	70-75	5	782
Qpfc3	80-90	4	13 2

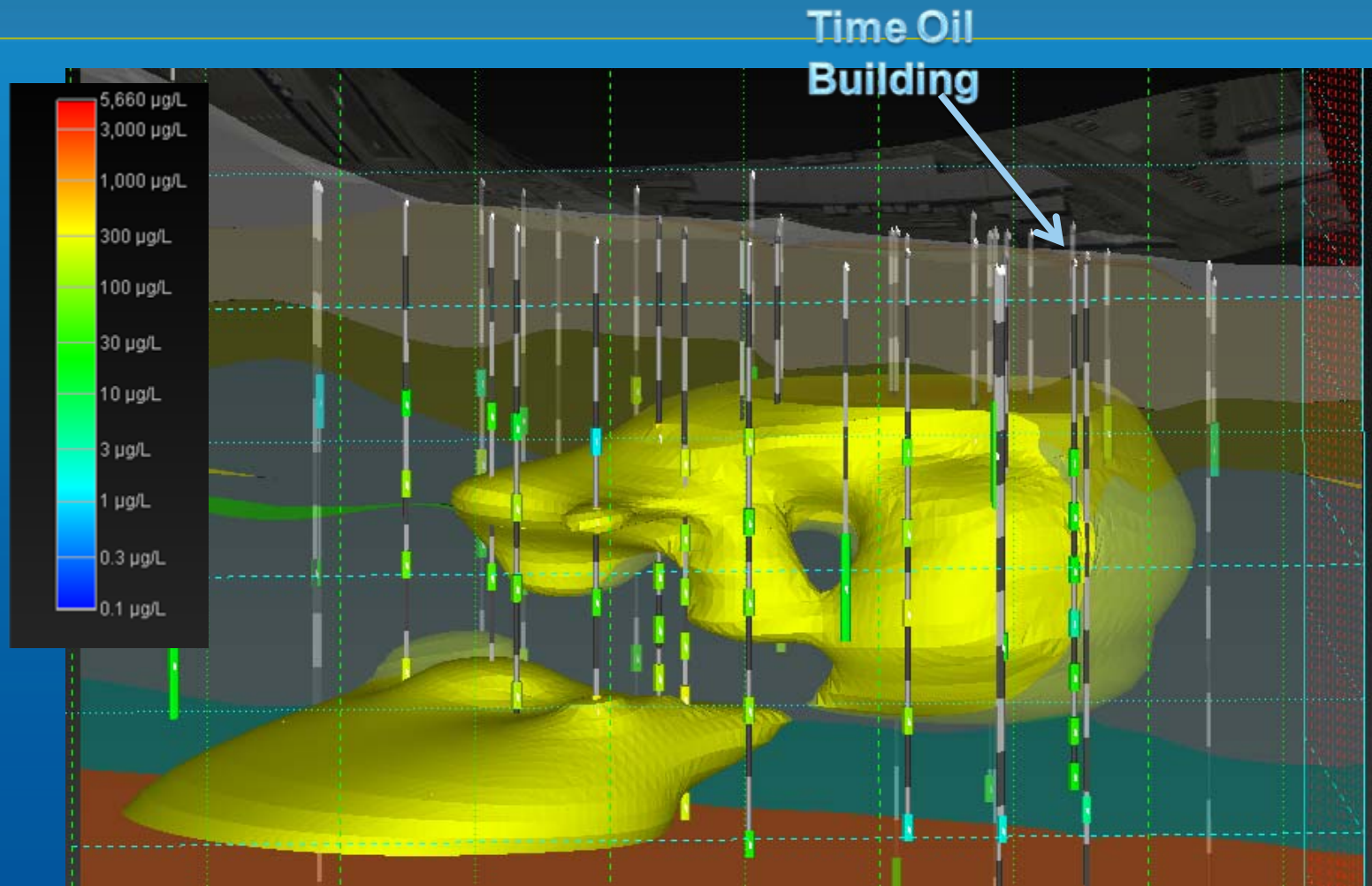
Vertical Stratification of the Groundwater Contaminant Plume

Legend

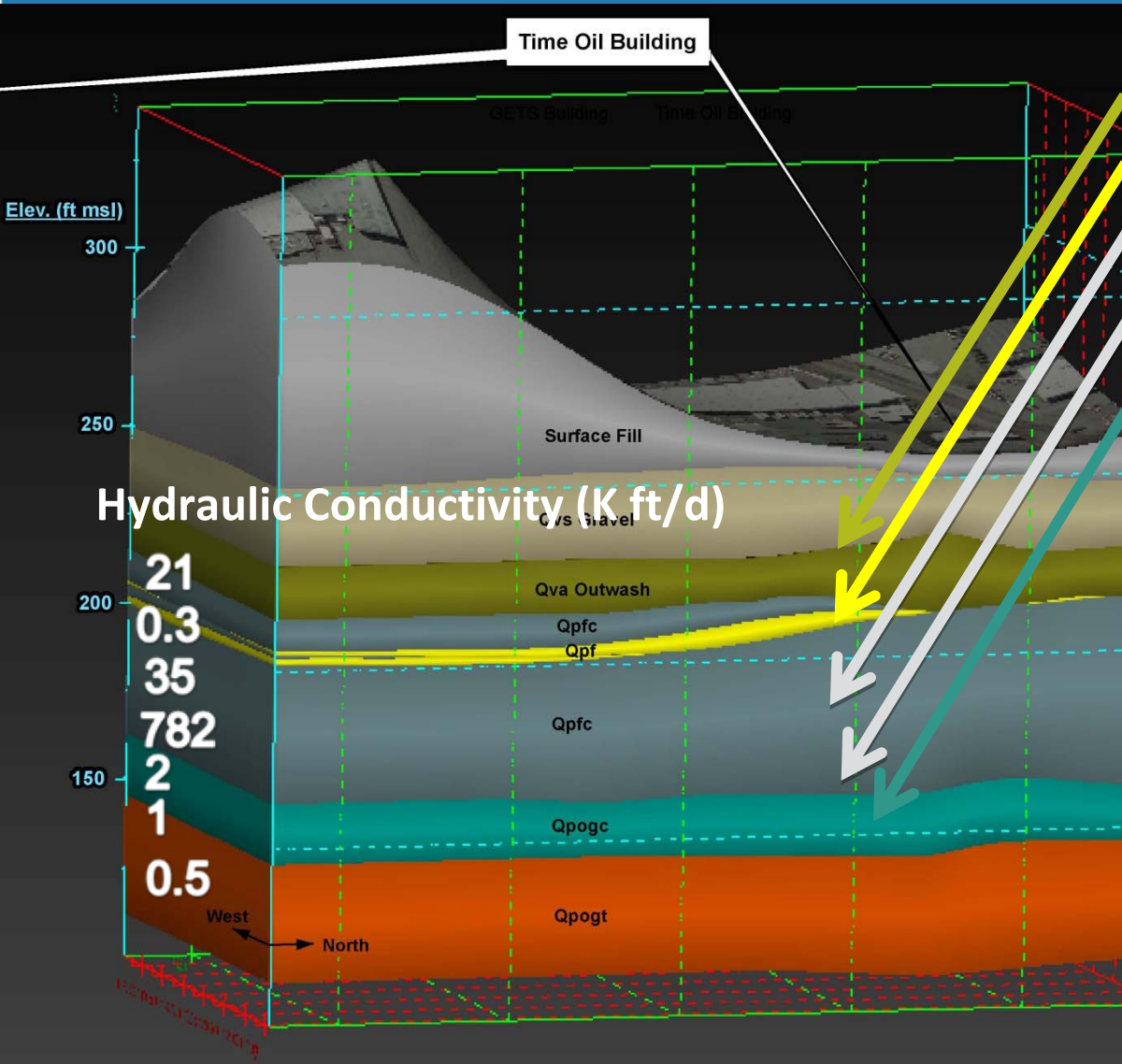
- Vertical Profile Location
- 2011 RDI Boring
- ⊕ Groundwater Monitoring Wells
- 300 ug/L Total COC Isoleth in Qva
- 300 ug/L Total COC Isoleth in Qpf
- 300 ug/L Total COC Isoleth in Qpfc
- 300 ug/L Total COC Isoleth in Qpogc



Cross Section of Contaminant Plume



Mass Discharge Across Transects



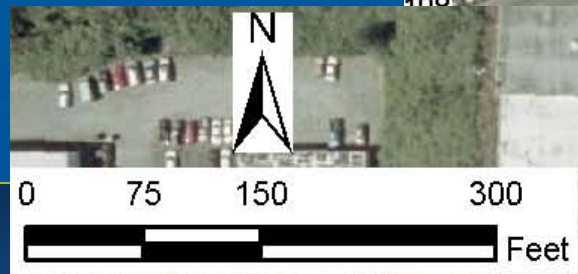
	Total VOC MD	
	(kg/yr)	% of Total MD
Transect 1		
Qva	0.1	1%
Qpfc1/Qpf	2.9	31%
Qpfc2	5.9	64%
Qpfc3	0.06	1%
Qpogc	0.3	4%
Total	9.3	
% of Total		
Transect 2		
Qva	0.01	0.4%
Qpfc1/Qpf	0.2	7%
Qpfc2	1.7	57%
Qpfc3	0.1	3%
Qpogc	1.0	33%
Total	3.0	

96%

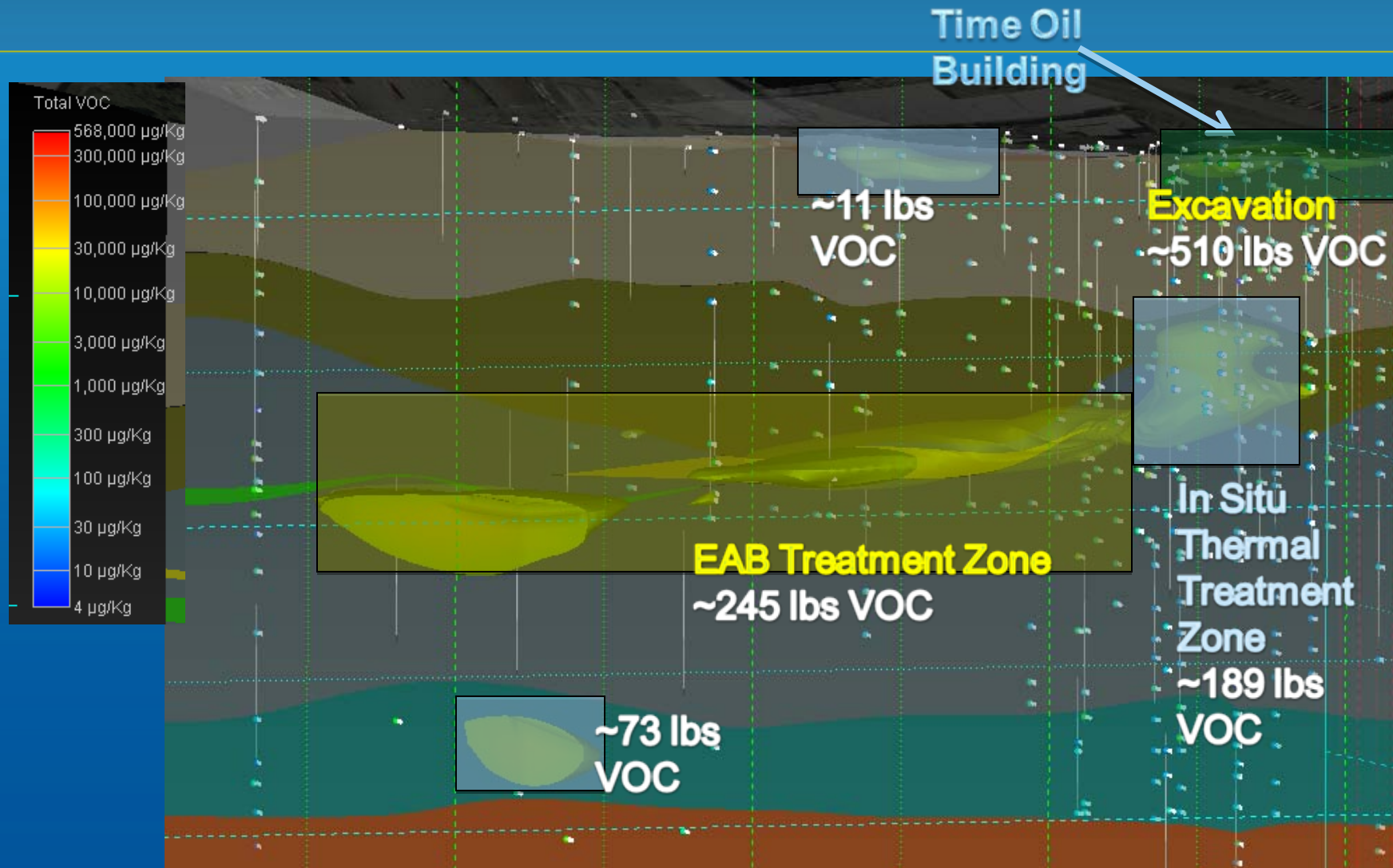
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Mapping Technologies

Zone	Surface Area (ft ²)	VOC Mass (kg)	% Discharge to GETS
Excavated Zone	3819	510	NA
Thermal Treatment Zone	11,746	~189	70 kg/yr
In Situ Bioremediation	162,005	~245	25 kg/yr



Treatment Zones: Selecting Vertical Intervals

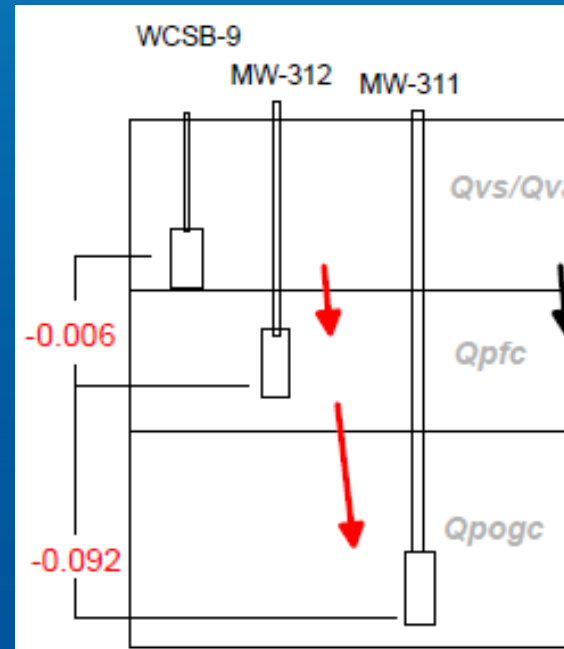
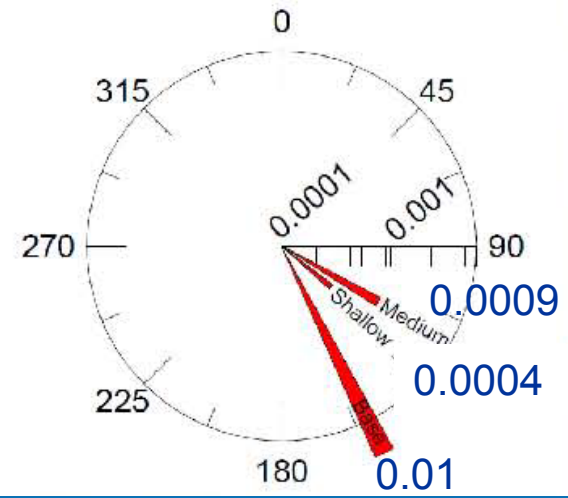


Challenges with Mass Discharge at Well 12A

- Assessing impacts from secondary sources, residual phase contaminants and back diffusion from low permeability layers.
- Managing complex hydraulics, including substantial changes in gradient magnitude and direction due to seasonal variations and operating Well 12A.
- Obtain realistic parameters such as porosity and hydraulic conductivity within vertically-discrete zones within the contaminant plume.

Site Gradient

Horizontal hydraulic gradient direction and magnitude with GETS off

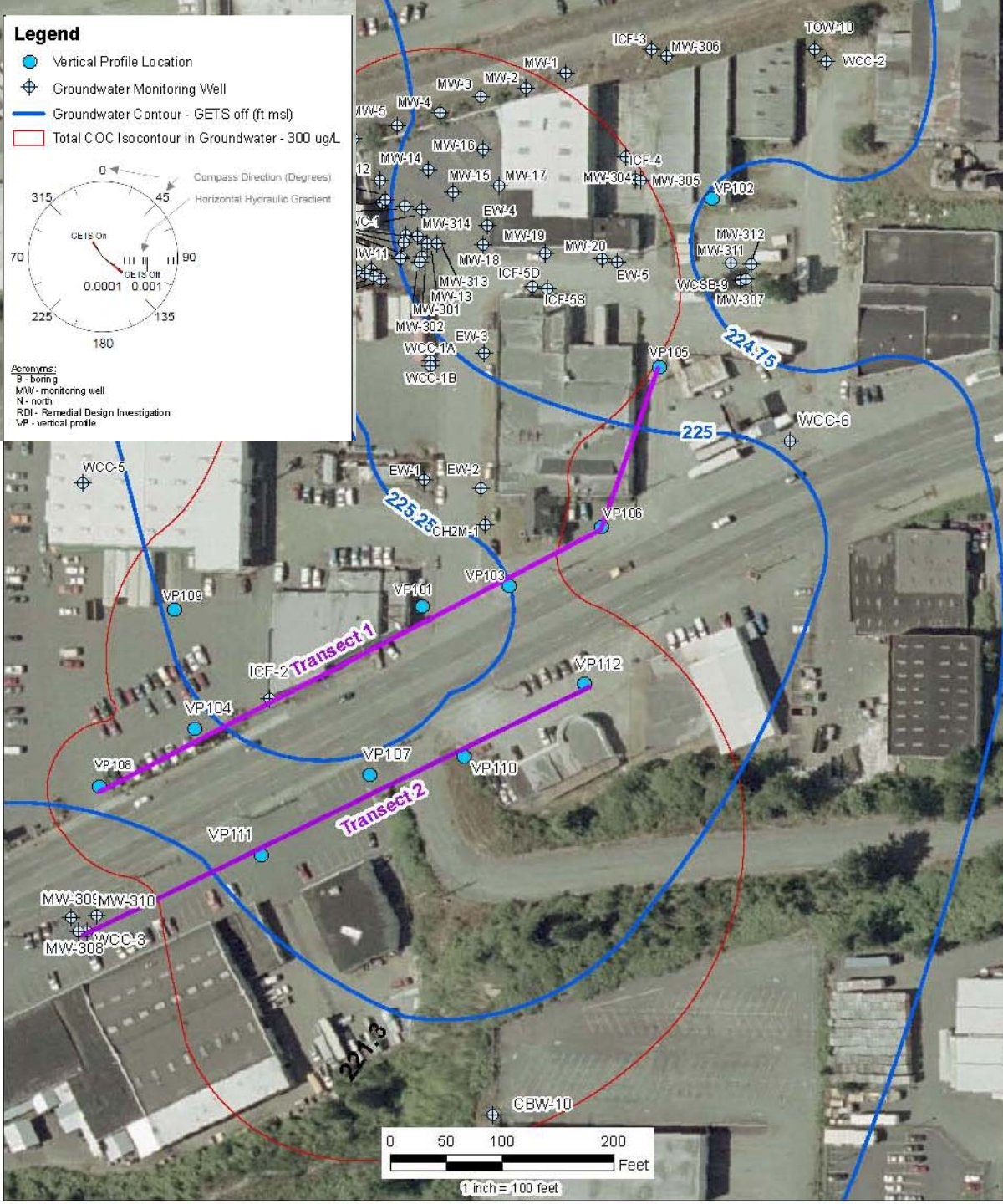


Legend

- Vertical Profile Location
- ⊕ Groundwater Monitoring Well
- Groundwater Contour - GETS off (ft msl)
- Total COC Isocontour in Groundwater - 300 ug/L

Compass Direction (Degrees)
Horizontal Hydraulic Gradient

Acronyms:
B - boring
MW - monitoring well
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Calculating Mass Discharge: Transect Method

Steps for Well 12A:

1. Draw polygons (use Theissen)
2. Calculate Darcy velocity (q) for each polygon: $q = K \cdot I$
3. Characterize polygon flux ($M_f = q \cdot C_n$)
4. Determine area ($W \cdot b = A$)
5. Evaluate mass discharge:

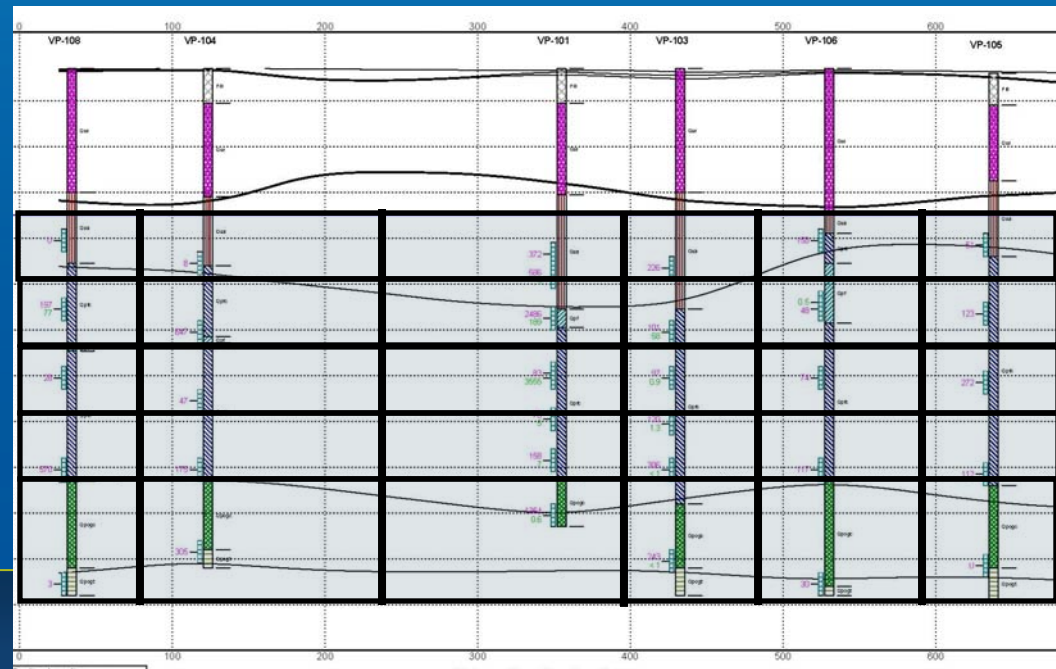
$$M_d = \sum (M_f \cdot A_n)$$

M_f = Mass flux

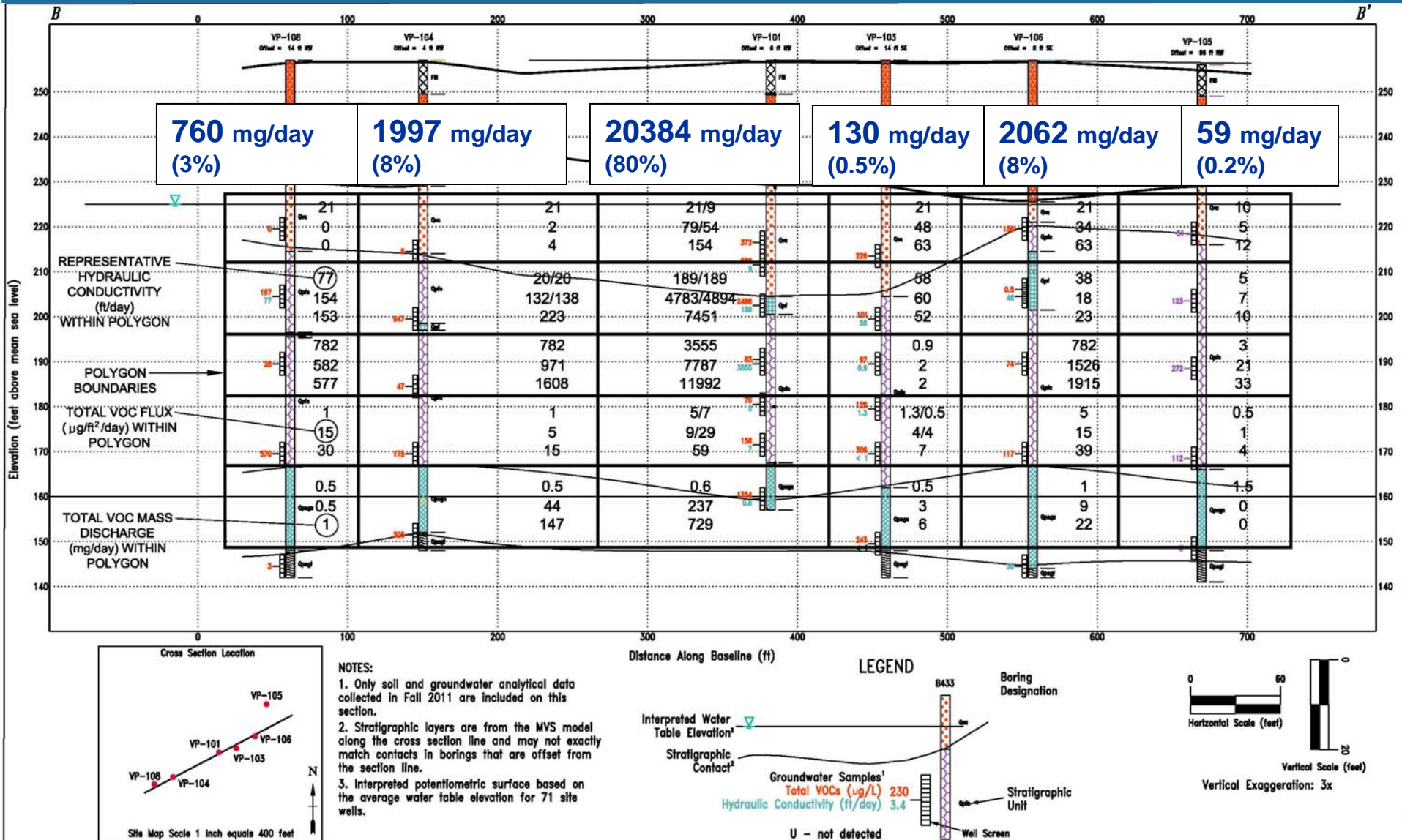
M_d = Mass discharge

C_n = concentration in polygon n

A_n = Area of segment n

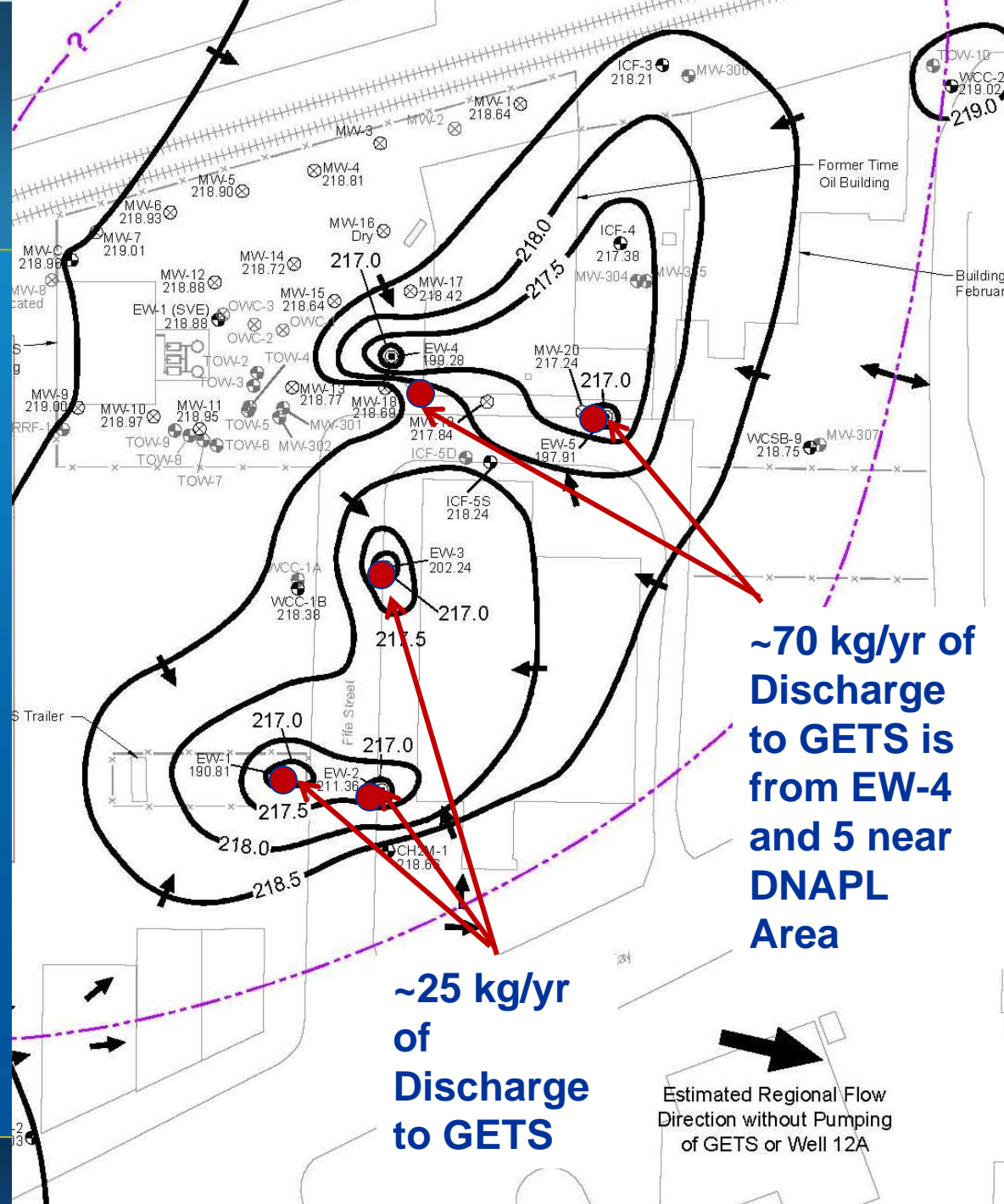


Transect 1



Mass Discharge: Pumping Test

- Capacity 500 gpm
- Screens 50-70 ft bgs
- Operation
 - EW-1, 40 gpm
 - EW-2, 8-16 gpm
 - EW-3, 7-9 gpm
 - EW-4, 6-15 gpm
 - EW-5, 6-12 gpm
- Mass Rate Treated (kg VOCs/yr)
 - EW-1, 4-8
 - EW-2, 4-12
 - EW-3, 8-12
 - EW-4, 24-48
 - EW-5, 24-48



**~70 kg/yr of
Discharge
to GETS is
from EW-4
and 5 near
DNAPL
Area**

**~25 kg/yr
of
Discharge
to GETS**

Estimated Regional Flow
Direction without Pumping
of GETS or Well 12A

Site Specific Uncertainties with Pumping Method

Uncertainty

- Pumping induced changes to natural flow regime
- Impacts of secondary sources on mass discharge assumptions
- Increase gradients through significant contaminant sources

Impact to the Estimate

- Potential to draw water from low permeability zones that would not normally contribute mass flux
- Potential to enhance dissolution/diffusion from sources increase estimates
- Potential that mass discharge from “sources”, i.e. Q_{pog_c} and Q_{pf_c} downgradient of pumping wells not accounted for.

What's Next?

- Assess critical information needed to determine if can use GETS to evaluate mass discharge,
- Determine if additional field data is needed to evaluate mass discharge methods,
- Pick a mass discharge measurement method,
- Measure baseline mass discharge,
- Implement ISTR, and EAB remedial actions to achieve mass discharge reduction goal,
- Two post-RA mass discharge,
 - 1st ~18 months post-Bioremediation,
 - 2nd contingency if additional Bioremediation needed to achieve objective.

Conclusions

- Mass Flux and Mass Discharge can improve management of complex contaminant sites and new technologies are increasing the confidence in these metrics.
- Use of new technologies has significantly improved remedial decision-making in developing, designing and implementing Remedial Actions.
- Well 12A will be a case study in how to use these approaches under the Superfund regulatory framework.

Questions and Answers

