

Case Study for the Use of a Decision Support Tool: Evaluating the Applicability of Remediation by Natural Attenuation Using BIOSCREEN at the Administration Area Naval Exchange (NEX) Gas Station, Naval Air Station Lemoore, Lemoore, California

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FOREWORD

This case study is one in a series designed to provide information on use of decision support tools that support the use of data, models, and structured decision processes in decision-making. These case studies include reports on selected tools that have been used to support activities such as site assessment and remediation, data management and visualization, and optimization. They are prepared to offer operational experience and to further disseminate information to project managers, site owners, environmental consultants, and others who wish to screen decision support tools and benefit from their previous use at sites.

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TABLE OF CONTENTS

<u>Section</u>	<u>Page</u>
NOTICE	i
FOREWORD.....	ii
ACKNOWLEDGEMENTS	ii
1.0 SITE BACKGROUND	1
2.0 USE OF DECISION SUPPORT TOOLS	3
3.0 LESSONS LEARNED	7
4.0 POINTS OF CONTACT	9
5.0 REFERENCES.....	9

FIGURES

Figure

1	SITE AND WELL LOCATION MAP.....	2
2	BIOSCREEN NATURAL ATTENUATION DECISION SUPPORT SYSTEM.....	7
3	DISSOLVED HYDROCARBON CONCENTRATION ALONG PLUME CENTERLINE IN MG/L.....	8

TABLES

Table

1	COMPARISON OF GEOCHEMICAL PARAMETERS AT SITE WITH AFCEE DATABASE.....	5
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1.0 SITE BACKGROUND

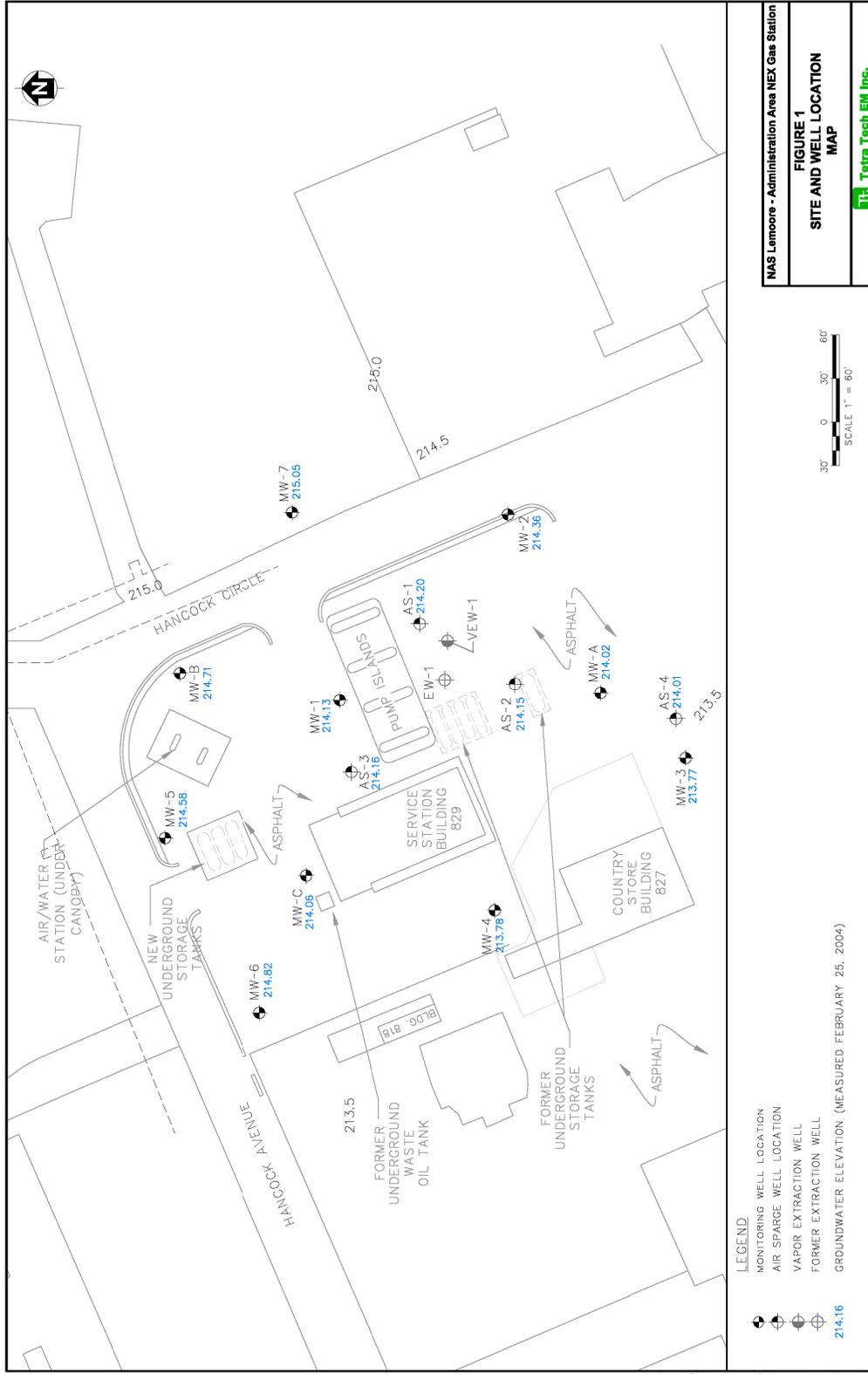
The Administration Area Naval Exchange (NEX) gas station at Naval Air Station (NAS) Lemoore was built in 1962. The fuel storage and distribution system at the gas station consisted of five 10,000-gallon gasoline underground storage tanks (USTs), one waste oil UST, and associated piping. The USTs were installed in 1974, and a release of gasoline from the USTs and associated piping was discovered in 1988. Floating free product (up to 9 inches) was observed during the excavation and initial investigation of the UST in 1988. The area affected by free product covered 18,000 square feet and was located directly north and south of the pump islands. More than 10,000 gallons of free product (gasoline) were removed from extraction well (EW)-1 between 1989 and 1994. In 1995, the five USTs were removed, and the tank excavations were backfilled with native soil. Three new USTs were installed in the northern portion of the site and are currently in use. Figure 1 shows the layout of the site.

Near-surface geology consists primarily of silts and clays with lesser amounts of silty sands. Interbedded silt and clay predominate from ground surface to approximately 16 feet below ground surface (bgs). Moderately graded, fine- to medium-grained sands are present below 16 feet bgs. Early estimates of permeability for near-surface soils were in the range of 4.2×10^{-5} to 1.41×10^{-4} centimeters per second (cm/sec) (Krazan 1989). Based on improved understanding of site lithology, this permeability is appropriate for silt and clay; however, the permeability of the sand layer is estimated to be higher (approximately 1×10^{-3} cm/sec). Depth to water beneath the site averages 4 feet bgs. The horizontal gradient is relatively flat (0.002 to 0.003 feet per foot) and is oriented to the southwest.

The constituents of concern include benzene, toluene, ethylbenzene and xylene (BTEX) and methyl tert butyl ether (MTBE.) The highest concentrations of MTBE and BTEX were detected in samples from well MW-1. Floating product was historically present in this well; however, no measurable product has been observed recently, and only a thin sheen of gasoline was observed in April 2003. Samples collected from wells AS-2 and MW-A also exhibit elevated concentrations of benzene and MTBE.

In general, concentrations of fuel constituents have remained stable over time. Concentrations of MTBE in well MW-1 fluctuate; however, in general, they remain greater than 100 milligrams per liter (mg/L). Very low concentrations of MTBE and benzene were detected in a sample from well AS-4, indicating that fuel is likely migrating toward the south-southwest within more permeable sand layers below 16 feet bgs. (Well AS-4 is screened from 20 to 25 feet bgs in a sand interval that is fairly continuous beneath the site.) Samples from wells located at the perimeter of the site, (MW-3, MW-4, and MW-B) contained no BTEX, MTBE, or total petroleum hydrocarbon (TPH) constituents.

FIGURE 1
SITE AND WELL LOCATION MAP



A risk assessment conducted in 2003 indicated that corrective action was warranted at the NEX gas station based on the levels of BTEX and MTBE in soil and ground water.

2.0 USE OF DECISION SUPPORT TOOLS

Remediation by natural attenuation relies on natural attenuation (NA) processes to achieve site-specific remedial objectives within a timeframe that is reasonable compared with other methods (U.S. Environmental Protection Agency [EPA] 1998). The applicability of using NA as the remedy for the Administrative Area NEX gas station at NAS Lemoore in Lemoore, California, was evaluated because the site fulfills many of the requirements for monitored natural attenuation (MNA) to be considered as a remedial approach. Office of Solid Waste and Emergency Response (OSWER) Directive 9200.4-17 identifies three lines of evidence that can be used to demonstrate the efficacy of MNA. The first line of evidence – evaluating historical soil and ground water chemistry data to demonstrate a meaningful trend of decreasing contaminant mass or concentration over time – was inconclusive. The second line of evidence – using hydrogeologic and geochemical data to demonstrate that NA processes are active and estimate degradation rates – can be developed using BIOSCREEN (<http://www.epa.gov/ada/csmos/models/bioscrn.html> - AFCEE 1997). (The third line of evidence – using field or microcosm studies to directly demonstrate the occurrence of a particular NA process – only required if the first two lines are inconclusive). This case study demonstrates the use of BIOSCREEN to evaluate NA processes at the NEX site.

Review of Conceptual Site Model

Three aspects of the conceptual site model (CSM) that must be identified to provide input values for the BIOSCREEN model are the timing of release, the configuration of the source term, and the soluble mass remaining in the soil of the source zone. The site stratigraphy must also be identified to run the model.

The timing of the release is not known. The tanks were installed in 1973, and the leak was first discovered in 1988; therefore, reasonable estimates of the time since release range from 16 to 31 years.

The configuration of the source term is difficult to estimate. The only reported location of a release is a joint in one of the product lines between the tanks and the pump island. The product odor was reported first at the cashier's booth, located north of the fueling islands, and the highest concentrations of BTEX and MTBE are found at a well north of the fueling islands (well MW-1). The distribution of high concentrations of benzene (above its effective solubility) — which encompasses the area below both the

former tank pits, distribution piping and the fueling island — suggests that product likely filled both tank pits and the distribution pipeline trenches at one time. Therefore, the source was modeled as located at the downgradient (southwest) edge of the tank excavation. The concentration of benzene in the closest borehole (24 milligrams per kilogram [mg/kg]) was used as a source concentration.

The soluble mass of hydrocarbon constituents is required as an input for modeling. The source volume for both simulations was obtained by multiplying the cumulative length of the former pit sidewalls and distribution piping by a 4-foot wide “lateral impact zone” and a 6-foot thick “vertical smear zone” to estimate the soil volume that may be affected by residual product. The result was multiplied by an assumed bulk density for soil of 1.7 grams per cubic centimeter (g/cm^3) and an average benzene concentration of 37 mg/kg in soil at the source area, to yield an estimate of 20,000 kilograms of soluble mass in the source area.

Borehole logging suggests that the shallow aquifer must be separated into two vertical components, or “zones.” The upper zone is characterized by alternating beds of silt and clay between the water table (approximately 4 to 5 feet bgs) and a depth of 16 feet bgs. The lower zone consists of a well-sorted, medium-grained sand channel deposit between depths of 16 and 26 feet bgs. The channel extends at least to the southern extent of the site. The difference in geologic characteristics between the upper and lower zones required estimating two sets of hydrogeologic parameters and two separate BIOSCREEN model runs.

Evaluation of Field Geochemical Data

The geochemical evaluation of the site indicates that the components of BTEX have been undergoing biodegradation. BIOSCREEN, which follows the Air Force Center for Environmental Excellence (AFCEE) NA protocol, uses the change in geochemical indicator concentrations observed between background and in-plume wells as a direct indication of mass reduction caused by biodegradation (AFCEE 1997). Changes in five geochemical indicators are tracked in the protocol: dissolved oxygen, nitrate, ferrous iron, sulfate, and methane. Oxygen, nitrate, and sulfate are electron acceptors that are consumed, along with BTEX, by microorganisms in biologically mediated redox reactions. Ferrous iron and methane are metabolic byproducts that are produced by similar reactions. Table 1 summarizes site geochemical data for in-plume and background wells and shows the observed changes in concentration of these geochemical parameters between source area and in-plume wells at the site.

TABLE 1

COMPARISON OF GEOCHEMICAL PARAMETERS AT SITE WITH AFCEE DATABASE

Parameter	Site Values		Observed Change in Concentration	AFCEE Database		
	Background	Source Area		Max.	Median	Min.
DO	1.6	0.1	1.5	12.7	5.8	0.4
Nitrate	72	0.5	71.6	69.7	6.3	0.0
Iron (Fe ²⁺)	0.3	0.39	0.1	599.5	16.6	0.0
Sulfate	15,465	10,500	4,965	109.0	24.9	0.0
Methane	0.002	0.012	0.01	48.4	7.2	0.0

Notes:

All units are milligrams per liter (mg/l)

Bold values are greater than any value in the AFCEE database.

Change in concentration represents background minus source area, except for iron and methane, where it represents source area minus background.

The changes in these five geochemical indicators are critical input parameters to BIOSCREEN. This is a spreadsheet-based analytical model based on the Domenico analytical solute transport model. The changes in concentrations of geochemical indicators are input to BIOSCREEN and then divided by chemical-specific utilization factors (stoichiometric ratios that relate the change in mass of these geochemical parameters to the decrease in mass of BTEX) to estimate the biodegradation capacity of the site.

In addition, the BIOSCREEN manual provides information about the concentrations of the five geochemical indicators based on a compilation of data from 28 AFCEE sites (referred to in Table 1 as the AFCEE database). These data are provided to show how they compare with the conditions observed at the Admin Area NEX site. The value for sulfate is significantly greater than the level reported in the AFCEE database. This high value reflects the highly saline nature of the shallow aquifer at NAS Lemoore. The high concentrations of nitrate and sulfate will theoretically provide a nearly inexhaustible supply of electron acceptors to drive anaerobic biodegradation.

BIOSCREEN Modeling

BIOSCREEN was run for both aquifer zones (upper and lower). BIOSCREEN requires entry of hydraulic, dispersion, sorption, and biodegradation (discussed above) parameters in addition to the source information. Hydraulic parameters were either calculated from site data (gradient) or from literature

values for the lithologic materials (hydraulic conductivity and porosity). Sorption parameters were also based on literature values, specifically the “typical” soil (soil bulk density and fraction of organic carbon) and chemical-specific (organic carbon partition coefficient) parameters listed in the BIOSCREEN manual. Longitudinal dispersion is typically assigned a value equal to one-tenth of the estimated plume length, but was doubled to one-fifth the estimated plume length to account for uncertainty in longitudinal movement of the source itself. Ground water sample results from April 2003 were used for the observed concentrations of BTEX in the upper (wells MW-A and MW-3) and lower (wells AS-2 and AS-3) zones. In both zones, the BTEX plume is primarily composed of benzene. The observed benzene concentrations decrease from greater than 1 mg/L to less than 0.2 microgram per liter from the near-source to more distant well in both zones.

BIOSCREEN output consists of curves that show concentrations of benzene versus distance along the centerline of the plume, as predicted based on three different modeling conditions: (1) no degradation, (2) first-order decay rate, and (3) instantaneous reaction. In each case, the modeled curves incorporate the effects of advection, dispersion and adsorption on BTEX concentrations, the only differences are if and how biodegradation is incorporated. Site data are plotted against the curves (cross-markers at distances of 30 feet and 70 feet) to compare observed concentrations versus modeled concentrations. The “no degradation” curve shows the expected concentrations if biodegradation is not active. The first-order decay rate model requires the user to specify a contaminant half-life. A conservative value of 2 years was used in this evaluation. The instantaneous reaction model is based on the geochemical input parameters and reaction stoichiometry described earlier in this section.

The BIOSCREEN input screen for the lower zone model is shown on Figure 2. The benzene output curves for the lower zone are depicted in Figure 3. Each zone was modeled separately because the seepage velocity is estimated to be five times faster in the lower zone than in the upper zone. A simulation time of 31 years was used for this simulation. (The user can estimate time of remediation by running the model with different simulation times until concentrations drop below the remedial goal at a specific point on the plume centerline.)

The results for the lower zone (Figure 3) indicate that concentrations of benzene are lower in the aquifer downgradient of the source area than would be expected if no biodegradation was occurring; however, the rate of biodegradation is much less than is predicted by the instantaneous reaction model. The results in the upper zone were similar, except both the first-order decay model and the instantaneous reaction model overpredicted the rate of biodegradation (modeled concentrations were lower than actual concentrations).

FIGURE 2

**BIOSCREEN NATURAL ATTENUATION DECISION SUPPORT SYSTEM
(BIOSCREEN Parameter Input Page – explanation of cell shading in upper right corner)**

BIOSCREEN Natural Attenuation Decision Support System
Air Force Center for Environmental Excellence Version 1.4

NAS Lemoore
Admin NEX IZ
Run Name

Data Input Instructions:
 115 → 1. Enter value directiv... or
 ↑ or 2. Calculate by filling in grey
 0.02 → cells below. (To restore
 formulas, hit button below).
 Variable* → Data used directly in model.
 20 → Value calculated by model.
 (Don't enter any data).

1. HYDROGEOLOGY
 Seepage Velocity* V_s 5.4 (ft/yr)
 or
 Hydraulic Conductivity K 1.0E-08 (cm/sec)
 Hydraulic Gradient i 0.0013 (ft/ft)
 Porosity n 0.25 (-)

2. DISPERSION
 Longitudinal Dispersivity* α_x 12.0 (ft)
 Transverse Dispersivity* α_y 1.2 (ft)
 Vertical Dispersivity* α_z 1.2 (ft)
 or
 Estimated Plume Length L_p 60 (ft)

3. ADSORPTION
 Retardation Factor* R 1.3 (-)
 or
 Soil Bulk Density ρ 1.7 (kg/l)
 Partition Coefficient K_{oc} 38 (L/kg)
 Fraction Organic Carbon f_{oc} 1.0E-3 (-)

4. BIODEGRADATION
 1st Order Decay Coeff* λ 3.5E-1 (per yr)
 or
 Solute Half-Life t_{half} 2.00 (year)
or Instantaneous Reaction Model
 Delta Oxygen* DO 1.52 (mg/L)
 Delta Nitrate* NO_3 71.55 (mg/L)
 Observed Ferrous Iron* Fe^{2+} 3.87 (mg/L)
 Delta Sulfate* SO_4 4965 (mg/L)
 Observed Methane* CH_4 0.01 (mg/L)

5. GENERAL
 Modeled Area Length* 100 (ft)
 Modeled Area Width* 60 (ft)
 Simulation Time* 31 (yr)

6. SOURCE DATA
 Source Thickness in Sat Zone* 6 (ft)
 Source Zones:
 Width* (ft) Conc. (mg/L)*
 50 24
 0 0
 0 0
 0 0
 50 24

Vertical Plane Source: Look at Plume Cross-Section and Input Concentrations & Widths for Zones 1, 2, and 3

Source Half-life (see Help):
 600 >1000 (yr)
 Inst. React. 1st Order
 Soluble Mass 20000 (Kg)
 In Source NAPL, Soil

7. FIELD DATA FOR COMPARISON
 Concentration (mg/L) 1.2 0
 Dist. from Source (ft) 0 10 20 30 40 50 60 70 80 90 100

View of Plume Looking Down
 Observed Centerline Concentrations at Monitoring Wells
 If No Data Leave Blank or Enter "0"

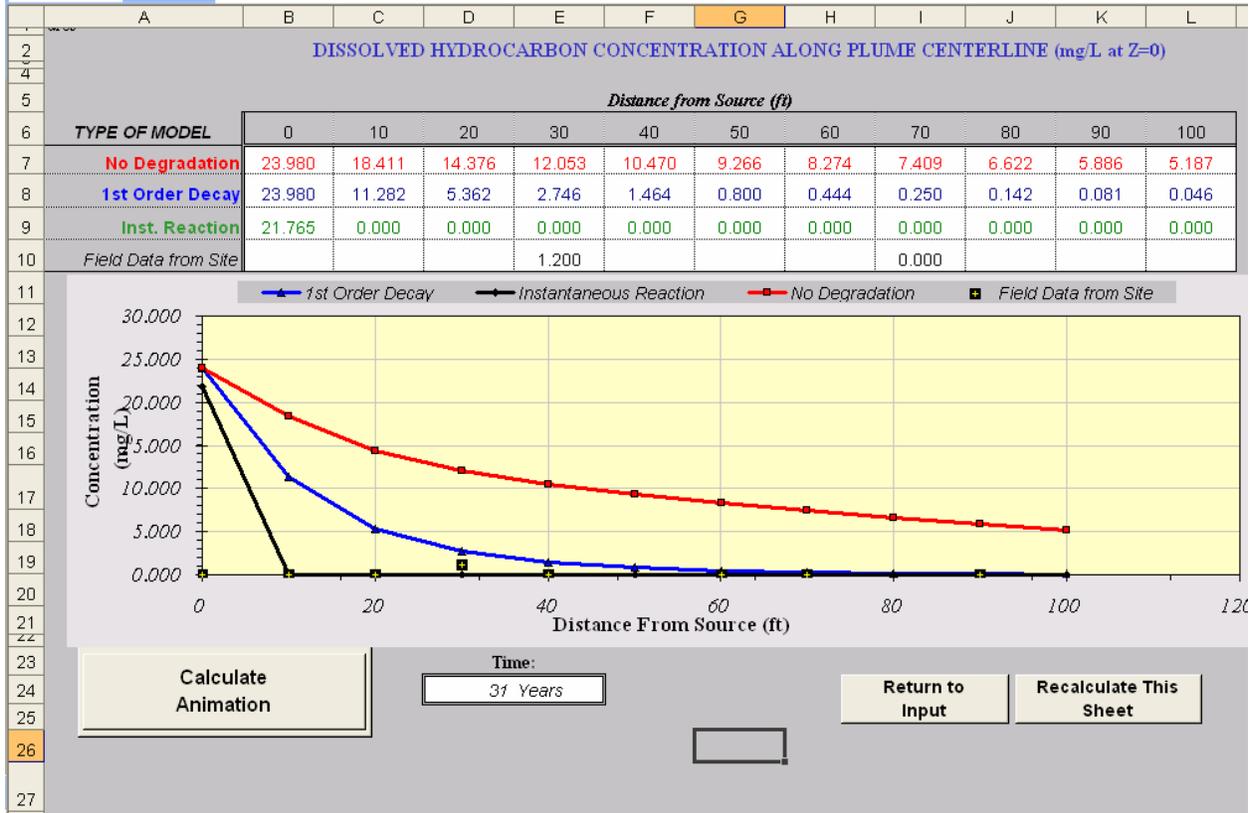
8. CHOOSE TYPE OF OUTPUT TO SEE:

RUN CENTERLINE **RUN ARRAY** **Help** Recalculate This Sheet
 View Output View Output Paste Example Dataset
 Restore Formulas for Vs, Dispersivities, R, lambda, other

3.0 LESSONS LEARNED

The first-order decay model seems to be the best predictor of actual conditions, as indicated by the reasonably close fit between observed and simulated values on Figure 3. However, the lower-zone model provides a better fit than the upper-zone model. This outcome may be caused by uncertainty in the dimensions and concentration of the soluble mass. Fluctuations in the water table change saturation conditions in the source area, which introduces significant error in estimating the dimensions of the source term. The upper zone is in direct contact with the source; therefore, the upper zone plume is likely to be much more sensitive to inaccuracies in the source term.

FIGURE 3
DISSOLVED HYDROCARBON CONCENTRATION ALONG PLUME CENTERLINE
IN MG/L
(BIOSCREEN Output Page)



Note: The upper (red) curve shows the estimated change in concentration of dissolved hydrocarbons assuming no degradation. The middle (blue) curved line shows the estimated change in concentration of dissolved hydrocarbons assuming first-order decay. The lower (black) curve shows the change in concentration of dissolved hydrocarbons calculated by the instantaneous reaction model. Crosshair markers at 30 and 70 feet show observed concentrations (marker at 70 feet represents a nondetected result at well AS-3, at a detection limit of 0.2 µg/L).

For this application, the instantaneous reaction model does not fit the actual site data well and appears to be a poor predictor of site conditions. The model suggests that the entire dissolved hydrocarbon plume is biodegraded almost as soon as it enters the aquifer. The majority of the biodegradation capacity of the aquifer is provided by the extremely high concentrations of sulfate; enough sulfate is present to degrade all of the BTEX, based on the stoichiometric relationship between the hydrocarbons and the electron acceptors. However, BIOSCREEN does not take oxidation-reduction potential (ORP) into account and the user must consider the effects of ORP on biodegradation in an analysis external to the BIOSCREEN model. Based on limited data at the site, the ORP is not below the upper threshold (- 250 millivolts) regarded as necessary for sulfate reduction.

BIOSCREEN was used to evaluate whether the dissolved BTEX plume at the Administration area NEX could be remediated through natural attenuation within a reasonable timeframe. BIOSCREEN can be used to obtain an estimate of remedial timeframe at any point along the plume centerline by iteratively running the model with different values of simulation time and noting when the concentration at the point of compliance is less than the action level. In this case, the remedial timeframe clearly is unreasonable. Biodegradation of BTEX appears to be occurring, based on the relationship of the “no decay” curve to the observed data, but the dissolved plume will likely remain for a long period (hundreds to thousands of years).

The BIOSCREEN input screen (Figure 2) indicates a possible explanation: the half-life of a residual source of this size may exceed 1,000 years (see the model-calculated source half life on the source data section of the input screen). The large soluble contaminant mass in the source zone may continue to bleed dissolved hydrocarbons to the aquifer during periods of high recharge or whenever the water table rises into the source zone soil. Because of this result, the project team recommended aggressive mass reduction measures in the corrective action plan (CAP), rather than relying on MNA alone.

4.0 POINTS OF CONTACT

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