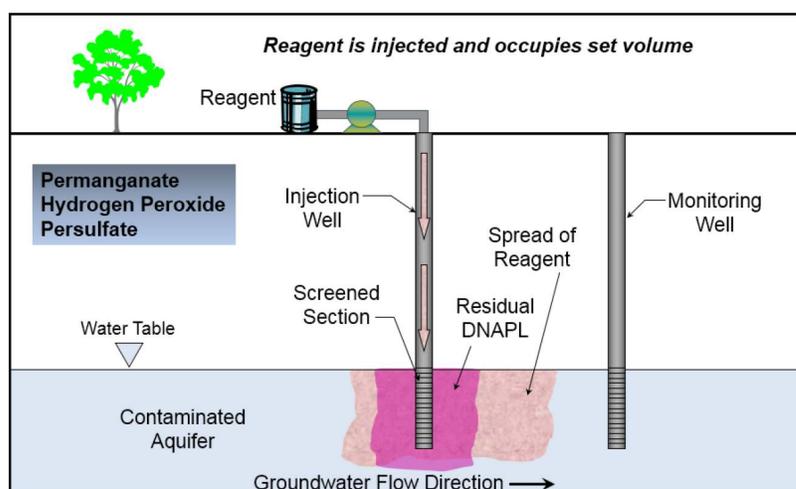


In Situ Chemical Oxidation

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Schematic



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In Situ Chemical Oxidation

Introduction

In site chemical oxidation (ISCO) is an in situ remediation technology that involves the injection of chemical oxidants into the subsurface, the most common of which are permanganate, persulfate, and hydrogen peroxide. ISCO is applicable to treat a wide-range of contaminants of concern (COCs) including chlorinated ethenes and ethanes, petroleum hydrocarbons and their constituents, 1,4-dioxane, energetics, pesticides, and phenols among others. ISCO also can facilitate the removal of non-aqueous phase liquids (NAPLs). It is important to select an appropriate oxidant, dosing, and activation agent (if needed) based on the COCs present since not all compounds can be treated effectively by a single oxidant.

Other Technology Names

ChemOx

Chemical oxidation

Description

ISCO is a remediation technology involving the injection and distribution of a chemical oxidant into the subsurface to transform COCs in groundwater and soil into innocuous byproducts. It can be considered for contaminant mass removal at sites where groundwater and/or porous media contain COCs such as petroleum hydrocarbons, chlorinated solvents, 1,4-dioxane, and energetic compounds, which are amenable to oxidation.

Oxidants

A variety of ISCO reagents are available on the market including hydrogen peroxide, sodium persulfate, potassium permanganate, sodium percarbonate, potassium permanganate, and sodium persulfate, which generally are applied in liquid form.



1 Oxidants normally shipped in solid form, such as potassium permanganate or sodium persulfate, are dissolved easily and mixed on site to form a solution having the required design concentration. Design considerations for the

common oxidants are listed in the table below. The three most common oxidants are described in the paragraphs that follow.

Permanganate

Permanganate has been used for more than 50 years to treat contaminants in drinking water and wastewater. More recently, permanganate has been used as an oxidant to treat contaminated soil and groundwater. When permanganate reacts with organic contaminants, the contaminants are oxidized to carbon dioxide and the permanganate is reduced to a manganese dioxide salt and a potassium (or sodium) salt.

The reaction of permanganate is described by second order kinetics. The rate of reaction is dependent upon the concentrations of both the permanganate and the COCs as well as the concentrations of other competing species, such as reduced metals and natural organic matter. Hence, increasing the concentration of permanganate will increase the rate of reaction with the COCs and other competing species. Also, as the concentration of COCs are reduced over time, the rate of reaction decreases. Because permanganate reacts slowly in the aquifer, it is able to travel further from the injection point before it completely reacts compared to other oxidants.

Either potassium permanganate (KMnO_4) or sodium permanganate (NaMnO_4) can be used. KMnO_4 is a solid and its solubility in water is limited to 6% [wt/wt (SERDP/ESTCP, 2011)]. It is easily transported to the field where it can be mixed with potable water or groundwater to the desired concentration. KMnO_4 dust can be a health hazard that requires some control during mixing on site. Although KMnO_4 costs less than NaMnO_4 , it may require sophisticated equipment on site for dissolving and distributing. NaMnO_4 has a higher solubility in aqueous solution at approximately 40% (SERDP/ESTCP, 2011). It is typically transported to the site as a liquid and then diluted to the desired concentration. NaMnO_4 is more reactive in the presence of certain reductants and needs to be handled carefully.

Field applications of permanganate have generally consisted of 0.5 to 3.0% concentration of injected solution. Higher concentrations can be used, but sometimes lead to excessive manganese dioxide formation around injection points, which can clog both the injection point and the aquifer.

Persulfate

Persulfate ($\text{S}_2\text{O}_8^{2-}$) is delivered in the form of sodium persulfate. Sodium persulfate has a water solubility of approximately 40% and results in a clear

solution. It is very reactive and produces innocuous byproducts.

Persulfate reaction chemistry is complex. Oxidation can occur via electron transfer or free-radical pathways. It is most common to activate persulfate using elevated temperatures (35 to 40°C), creating strongly alkaline conditions (pH upwards of 10 or 12), with ferrous iron (Fe[II]), or with hydrogen peroxide (H₂O₂) to generate sulfate free radicals, which facilitate contaminant destruction.

Sodium persulfate is highly soluble (73 g/100 g H₂O at 25 °C), and the density of a 20 g/L solution at 25°C (1.0104 g/mL) is greater than water. Once injected, a highly-concentrated solution of Na₂S₂O₈ can be transported by density-driven and diffusive transport. In addition, it is stable in the subsurface, with half-lives of up to 700 days reported in the literature (SERDP/ESTCP, 2011). It has less affinity for natural organic matter than permanganate or peroxide; hence, less oxidant is required. Persulfate can oxidize benzene, while permanganate cannot. This allows persulfate to be used in the remediation of fuel spills and benzene, toluene, ethylbenzene, and xylene (BTEX)-contaminated groundwater. The generation of sulfate also can promote biodegradation of petroleum constituents under anaerobic conditions, which can be designed as a polishing step after ISCO is completed. Persulfate does not produce the heat and gas evolution involved with hydrogen peroxide application.

Hydrogen Peroxide

It has been recognized since the late 1800s that hydrogen peroxide in the presence of an iron catalyst creates a very strong oxidant, commonly known as Fenton's reagent or catalyzed hydrogen peroxide (CHP). Although hydrogen peroxide itself is a strong oxidizer that is capable of oxidizing organic compounds, when combined with ferrous iron, the iron serves as a catalyst to form highly oxidizing hydroxyl radicals, which have an oxidation potential twice that of hydrogen peroxide. The process consists of a number of reactions, which are complex and consist of a variety of initiating, propagating, and terminating steps. These reactions produce several types of free radicals including the hydroxyl radical (OH•), the perhydroxyl radical (HO₂•), and the superoxide anion (O₂•-), all of which have very high oxidation potentials. The free radicals oxidizes organic compounds into smaller hydrocarbons that are easily oxidized to carbon dioxide and water.

The optimal pH for the generation of hydroxyl radicals and for hydrogen peroxide stability is between 3.5 and 5.0. An acid, such as sulfuric or hydrochloric, is often added to the aquifer to create a desired acidic pH.

Alternatively, a chelating agent, such as sodium citrate, citric acid, or ethylenediamine tetra acetic acid (EDTA) can be added to control the rate of decomposition of hydrogen peroxide allowing the reaction to occur at a near neutral pH. CHP systems are designed to either introduce an iron catalyst, such as ferrous sulfate or ferric chloride, or to take advantage of the naturally occurring minerals in the subsurface. Common minerals such as goethite or hematite among others, have been documented to effectively catalyze the peroxide reaction (SERDP/ESTCP, 2011). Low loadings may not provide sufficient iron to initiate catalysis of the hydrogen peroxide, whereas high concentrations can reduce aquifer permeability and the rate of reactions that terminate the formation of the hydroxyl free radical. The required dose is based on a number of site- and application-specific factors including, but not limited to, the presence of naturally occurring iron in soil and groundwater, concentrations of organic matter and COCs, and the target concentration of hydrogen peroxide in the aquifer. Optimum concentrations are best determined by performing bench-scale treatability studies.

CHP can be used to oxidize both contaminated soil and groundwater. CHP systems have been designed to introduce concentrations of peroxide ranging from 0.5 to 12%. Concentrations at the lower end of the range (i.e., 0.5 to 1%) are used to treat dissolved-phase contamination, whereas higher concentrations are required at sites where sorbed or non-aqueous phase liquid (NAPL) is present. It is important to note that concentrations greater than about 10% can be problematic due to the exothermic nature of the reaction, which can significantly raise the temperature of the soil and create fire and explosion hazards. In addition, a substantial volume of gas can be generated that may cause surfacing of groundwater and reagents and potentially mobilize contaminants. Additional precautions and rigorous monitoring should be employed when using high concentrations.

Oxidant Delivery Approaches and Design Considerations

Delivery methods for liquid oxidants include direct push methods through wells or points and groundwater recirculation through horizontal or vertical extraction and injection wells. Combined approaches consisting of direct push in some locations and recirculation in others are sometimes used. Hydraulic fracturing can be used at sites where introduction into low permeability media is required. Regardless of the method used, repeat additions of the oxidant and any activation catalysts (e.g., ferrous sulfate, NaOH, etc.) typically are necessary to obtain substantial oxidation of the organic contaminant and achieve remedial goals.

Direct push methods are well-suited for consolidated materials and weathered bedrock because there tends to be sufficient interconnected pore space to permit the distribution of the amendment throughout the treatment zone. In low permeability materials, such as silt and clay, the radius of influence (ROI) may be limited and high pressure may develop and can compromise the integrity of the formation. In addition, there is a greater likelihood to displace contaminated groundwater compared to recirculation approaches. Application of oxidants using a direct injection approach typically occurs over a short time (minutes to hours) at each location. However, in some cases, it may be desirable to design systems using a gravity feed system to utilize gravity to continuously introduce the amendments into wells over an extended time. Temporary or permanent vertical wells can also be used for direct injection of liquid oxidants under low pressure or gravity feed. Wells are used for deeper applications (beyond 30 -50 feet), to reduce long-term delivery costs when multiple injection events are projected, or for treatment of bedrock geology.

Groundwater recirculation (injecting from certain wells and extracting from others) can be used to overcome some of the distribution challenges associated with direct injection. Recirculation systems are designed to extract groundwater, add and mix the reagents and substrates, and reinject the amended water into the aquifer. Regulatory requirements may require above-ground treatment of dissolved contaminants prior to re-injection. Recirculation and mixing of amendments into groundwater is commonly performed using permanent injection and extraction wells, although a combination of direct push points and permanent wells can be used. Recirculation of amended groundwater can be used to more cost effectively treat larger and deeper contaminated areas, especially involving more transmissive aquifer units. Systems also can be designed to facilitate distribution in heterogeneous and lower permeability aquifers where long-term matrix diffusion rebound is a concern. Recirculation minimizes displacement of contaminated groundwater compared to direct injection systems by creating flow pathways from the injection locations to the extraction locations. Some applications perform recirculation until a pre-determined pore volume of groundwater has been exchanged in the aquifer. The goal of this approach is to increase long-term distribution and persistence of the amendments throughout the treatment area and enhance dissolution of the DNAPL if present.

Solid amendments, such as permanganate, can be used to treat vadose zone soils. Solid oxidants can be mixed into vadose zone soils using various types of specially equipped backhoes or large diameter auger equipment. Introduction

of solid amendments into low permeability media can be enhanced using pneumatic fracturing techniques.

Understanding the characteristics of the subsurface is important when applying oxidants in situ. Distribution tends to be easier in sandy, more permeable and homogeneous aquifers. It is difficult to obtain adequate delivery volume and distribution of the oxidant in fine sand, silt and clayey materials and in heterogeneous aquifers containing multiple discrete lithologic units. In less permeable aquifers, injection points must be placed closer together.

Geochemical conditions including hardness, total organic carbon, dissolved organic carbon, pH, and contaminant concentration must be known in order to design the amendment distribution system and determine appropriate mass, concentration, and flowrate of amendments.

The concentration of oxidant used depends on the concentrations of contaminants and organic matter as well as the type of delivery approach applied. Typically, lower concentrations of oxidant can be used when injected via a recirculation approach, since oxidant is being continuously delivered to the treatment area, and higher concentrations can cause rapid deterioration of the delivery equipment. Higher oxidant concentrations need to be used for direct injections, since it is being introduced on a batch basis, and it may be desirable to minimize the volume of fluid injected to reduce the chance of displacing contaminated groundwater.

Monitoring and Data Interpretation

A variety of process monitoring must be performed while introducing and distributing oxidants and any associated activation agents. The flowrate, pressure, and temperature are measured at the injection manifold and/or each injection well/point to control injection delivery. Similar data are collected from the extraction well if a recirculation system is employed.

Several indicator parameters should be measured at a representative number of performance monitoring locations when injecting permanganate, persulfate, and hydrogen peroxide into the subsurface. These include groundwater quality parameters such as pH, conductivity, oxidation-reduction potential; groundwater elevations; and concentrations of potentially mobilized metals in groundwater (conversion of trivalent to hexavalent chromium is of particular concern for oxidation). These parameters are measured to evaluate distribution of the oxidant, as well as to determine hydrogeologic and geochemical changes, which may occur in the aquifer as a result of the oxidant application. Although these changes typically occur within the treatment area and return to

near baseline values shortly after the application, the aquifer geochemistry should be monitored to ensure that any nearby downgradient receptors are not impacted. A semi-qualitative evaluation of the concentrations of oxidants can easily be performed in real time using field test kits and/or a field spectrophotometer. The presence of permanganate in wells also can be determined by visual inspection (water becomes purple). Similarly, evidence of bubbles in groundwater and/or elevated groundwater temperatures may be indicative of the presence of peroxide in the vicinity of a monitoring well.

After each oxidant application is complete, longer-term performance monitoring should be performed (NAVFAC, 2015). This monitoring consists of measuring concentrations of COCs in monitoring wells at various time intervals to determine the degree of treatment and the need for additional injections. Periodic monitoring should be performed involving the same indicator parameters discussed above to assess whether the aquifer has returned to baseline conditions and any mobilized metals attenuate before reaching any sensitive receptors. Proper preservation procedures for groundwater need to be followed to neutralize any residual oxidant presence in collected groundwater samples to avoid ongoing reactions that can bias COC results low.

Development Status and Availability

The following checklist provides a summary of the development and implementation status of ISCO:

At the laboratory/bench scale and shows promise

In pilot studies

At full scale

To remediate an entire site (source and plume)

To remediate a source only

As part of a technology train

As the final remedy at multiple sites

To successfully attain cleanup goals in multiple sites

ISCO is available through the following vendors:

Commercially available nationwide

Commercially available through limited vendors because of licensing or specialized equipment

Research organizations and academia

Applicability

Contaminant Class Applicability Rating for ISCO

(Rating codes: ● Demonstrated Effectiveness, ◐ Limited Effectiveness, ○ No Demonstrated Effectiveness, I/D Insufficient Data, N/A Not Applicable)

Nonhalogenated VOC	Halogenated VOC	Nonhalogenated SVOC	Halogenated SVOC	Fuels	Inorganics	Radionuclides	Munitions	Emerging Contaminants
●	●	●	●	●	○	○	●	I/D

Regarding emerging contaminants, ISCO can be effective in-situ treatment method for 1,4-dioxane. Research into the treatment of PFAS by oxidation is still at a research stage. Initial bench-scale testing of oxidation of PFAS have yielded mixed results (e.g., shown to degrade PFOA, but not PFOS), with heat activated persulfate showing the most promise to date.

A list of specific compounds and the degree to which they are treated (E = excellent, G = good, P = poor) is provided in the table below. Permanganate, persulfate, and peroxide are well suited for application across a wide range of conditions; however, COCs and other site-specific conditions (e.g., soil lithology and hydrology, aboveground and belowground structures, nearby receptors)

and RGs must be carefully considered when selecting the most appropriate oxidant for a site.

Oxidant Applicability to Specific Contaminants (E = excellent, G = good, P = poor)			
Contaminant	Oxidant		
	Permanganate	Activated Persulfate	Activated Peroxide
Petroleum hydrocarbons	G	E	E
Benzene, toluene, ethyl benzene, xylenes	E	E	E
Phenols	G	E	E
Polycyclic aromatic hydrocarbons	G  <u>2</u>	E	E
Methyl tertiary butyl ether	P	E	E
Tert-butyl alcohol	NA	E	E
Chlorinated ethenes	E	E	E
Carbon tetrachloride	P	G	P
Chloroform	P	G	P
Methylene chloride	P	G	G
Chlorinated ethanes	P	G	G
Chlorobenzene	P	E	E
Polychlorinated biphenyls	P	P	P
Energetics (RDX, HMX, TNT)	E	G	G
Pesticides	G	G	P

1,4-dioxane	P	E	E
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NA - Not available

Source: Adapted from: In Situ Chemical Oxidation, EPA Engineering Issue Paper, Scott G. Huling and Bruce E. Pivets. August 2006.

Cost

ISCO can be a very cost-effective technology if properly designed and applied. Similar to many in situ remediation technologies, the most critical cost factors are associated with the contaminant mass to be treated, the nature and extent of contamination (i.e., size of the treatment area), and number of injection points/wells required. As with all in situ technologies, application costs vary according to site conditions and contaminants. Major cost drivers include:

Upfront Costs

- Need for bench-scale tests and/or pilot studies to demonstrate effectiveness at a particular site and determine relevant design parameters.
- Quantities of oxidant and activators required, which are dictated by the contaminant type and mass to be treated, type of oxidant used, treatment area, and site geochemistry.
- Lithology and hydrogeology: In particular, native SOD may vary from site to site, and this can affect oxidant consumption and ROI around injection points.
- Number of injection points/wells required, which is dictated by the contaminant mass to be treated, site hydrogeologic conditions, and area to be treated.
- Equipment (including need for permeability enhancement techniques) and labor to introduce and distribute the amendments, which is dictated by the application method and duration of each injection event.
- Areal extent of contamination and depth of contamination.
- Presence of above and below ground structures and utilities.

Operation and Maintenance Costs

- Frequency of reapplication of amendments. Normally two or more injection events are required (SERDP/ESTCP, 2011). However, site specific remedial cleanup goals (RGs) and levels contamination (e.g., presence of NAPL) can significantly impact the number of applications required. Sites with low permeability soil units are subject to matrix diffusion rebound, which can

drastically influence the number of injection events or ability to meet RGs given the shorter persistence times for ISCO amendments.

- Monitoring requirements after amendment addition.
- Treatment timeframe.

The list above highlights those cost dependencies specific to composting and does not consider the dependencies that are general to most remediation technologies. Click [here](#) for a general discussion on costing which includes definitions and repetitive costs for remediation technologies. A project-specific cost estimate can be obtained using an integrated cost-estimating application such as RACER® or consulting with a subject matter expert.

Duration

The duration of the field construction or amendment application for ISCO is relatively quick, ranging from a few days to a few weeks. This short duration is one of the attractive features of ISCO, especially at sites where disruption of ongoing facility operations is a concern.

The persistence of the oxidants in the aquifer after completing active injection varies based on the oxidant type, the concentration injected, and site-specific lithology and hydrogeology. Depending on SOD, permanganate can be the longest lasting oxidant, possibly persisting for up to a year at a site depending on concentrations injected and groundwater flow. Hydrogen peroxide is the least persistent of the oxidants described, generally lasting from a few days to one to two weeks. Persulfate typically persists for weeks to months, and is less influenced by SOD than permanganate or peroxide. Primary factors that influence the duration of the ISCO technology include:

- RGs
- Treatment methodology (i.e., source area treatment, dissolved plume treatment, containment)
- Presence of NAPL
- Number of injection events required
- Concentration of amendments applied

Most ISCO treatment applications require multiple injection events (typically three on average) to achieve site RGs (or treatment to the extent practicable). Treatment timeframes, however, can be decades for more complex remediation sites involving significant source area contaminant mass, large plumes, and/or

high initial dissolved phase contaminant concentrations. Because of the relatively short amendment persistence and resulting susceptibility to matrix diffusion rebound, ISCO can require more frequent injection events than other in situ amendment technologies. Once a point of diminishing returns is reached, the remedy may need to be transitioned to an alternative less-aggressive technology such as [enhanced in situ bioremediation](#) or [monitored natural attenuation](#) (MNA) and the groundwater monitored for contaminant rebound. Since it is often difficult to attain drinking water RGs in groundwater through ISCO treatment alone, the duration will also be dependent on the interim objectives established for the termination of injections and transition to an alternative remedial approach.

Implementability Considerations

The following are key considerations associated with applying ISCO:

- A primary limitation of ISCO relates to achieving adequate distribution and contact of the reagent with the COCs. Care must be taken to carefully design the injection system so that adequate contact is achieved. The ROI for ISCO reagents may be limited due to the reactive nature of the oxidants. Modeling using a reactive transport model can help address aquifer changes as the oxidant reacts with the COCs and aquifer materials. In general, a typical ROI for ISCO reagents may range from about 5 to 15 feet per delivery point.
- If an activating agent is used (i.e., iron, heat, alkaline, etc.), monitoring should be performed to gauge the distribution and ROI of the activating agent to ensure that the reagent is activated according to design. Activators may not be distributed the same distance as the oxidants due to different reaction rates, retardation factors, etc. In some cases, sequential application of the activator and oxidant may be more desirable than to apply the oxidant and the activator at the same time to minimize unproductive consumption of the reagents and alleviate health and safety issues.
- Site lithology and hydrogeology impact the technology's ability to achieve effective contact between the reagents and COCs. Heterogeneous soil lithology can limit the distribution of ISCO amendments, which can result in pockets of untreated residual contaminant mass throughout the treatment area. An aquifer hydraulic conductivity of 10^{-5} cm/sec or greater facilitates effective distribution.
- Soils should preferably have a low clay content to allow oxidant penetration.

- Moderate to high levels of immobilized NAPL and residual contaminant mass may be more cost effectively treated by other in situ technologies (e.g., in situ thermal treatment).
- Preferential flow paths can severely influence amendment distribution and result in pockets of untreated contaminant mass. Amendment distribution becomes more difficult and may be infeasible for lower permeability clay, highly layered, or heterogeneous subsurface environments. Higher injection pressures or permeability enhancement techniques (e.g., hydraulic or pneumatic fracturing) can improve distribution of amendments for these conditions.
- Change in oxidation states and/or pH can mobilize metals within the treatment zone.
- Permits are usually required to receive permission from state and federal agencies to conduct ISCO. The permits that may be required include a waiver of the underground injection control (UIC) requirements and an air quality permit if emissions are expected from exothermic reactions and heat generation.

In addition to the above-mentioned issues, there are a number of oxidant-specific considerations that are summarized in the table below.

Implementability Considerations for the Application of ISCO Amendments (adapted from NAVFAC, 2013 & 2015)	
ISCO Reagent	Injection/Distribution Design Considerations and Challenges
Permanganate	<ul style="list-style-type: none"> • Long-lasting in the aquifer; hence, both advection and diffusion processes contribute to distribution • Soil oxidant demand (SOD) can exceed the oxidant demand of the COCs by two to three orders of magnitude, and is usually the primary driver for the design amendment delivery volume. Consequently, it is critical to perform bench-scale testing of SOD as part of the design • Can persist and react with COCs several months after injections are complete, which helps to facilitate removal of the COCs and makes it an advantageous choice for biobarrier applications. This attribute also allows permanganate to travel greater distances under natural groundwater flow conditions to potentially increase the ROI of treatment beyond the injection distance

- Colors water purple, which can be observed easily in nearby surface water bodies and groundwater supply wells if distribution is not adequately controlled.
- At sites that contain highly acidic (low pH) groundwater, the manganese ion (Mn^{2+}) can persist for extended periods in the aquifer, which can result in an exceedance of a regulatory groundwater standard for manganese
- Manganese dioxide, an insoluble precipitate, is formed as a byproduct of the reaction, which can reduce the permeability of the aquifer. High concentrations of manganese dioxide have been reported to form when using permanganate to treat NAPL
- Presents a dust hazard
- Is not effective for treatment of light non-aqueous phase liquid (LNAPL) or dense non-aqueous liquid (DNAPL)

Persulfate

- Highly corrosive, thus compatibility of injection equipment with persulfate should be considered
- May require injection and distribution of additional reagents to activate (heat, strong bases, iron catalyst, chelating agent, hydrogen or calcium peroxide)
- Carbonate, bicarbonate, chloride, and other inorganic ions are reactive with radicals and may affect reaction efficiency and effectiveness
- Fe(II) oxidizes to Fe(III) and precipitates, thus reducing the activating capacity of the Fe(II) with time and distance
- The solubility of permanganate drops with temperature. Hence, the injection of a saturated solution prepared at ambient temperatures may form a precipitate when exposed to the cooler subsurface temperatures
- Sulfate can provide continuing bioremediation for petroleum contaminants under reducing conditions after oxidation reactions are exhausted
- The SOD can exceed the oxidant demand of the COCs. However, SOD typically is not as high as that of peroxide
- Persulfate can persist and react with COCs for two to three months after completing injections, which helps to facilitate removal of the COCs. However, it should be noted that the activating agent (i.e., heat, alkalinity, dissolved iron, hydrogen

peroxide) may not persist as long. Hence, the highly oxidative persulfate radical may not be generated

- A strong oxidant such as persulfate may be a better choice for treatment of source areas known to contain small amounts of NAPL mass

Hydrogen Peroxide

- Typically applied at concentrations ranging from 8 to 15%. Reaction is exothermic and generates gases. Greater concentrations increase risk of fire/explosion
- A large volume of oxygen is produced during decomposition of hydrogen peroxide, which displaces pore water and can increase ROI. Hence, lower pore volume design values are used compared to other oxidants
- Surfacing of fluids and vapor intrusion can occur due to the formation of a large volume of gas and heat generated
- Reagent is short-lived, which limits ability to distribute via diffusion processes
- Soil oxidant demand (SOD) can exceed the oxidant demand of the COCs by two to three orders of magnitude, and is usually the primary driver for the design amendment delivery volume. Consequently, it is critical to perform bench-scale testing of SOD as part of the design
- May require injection and distribution of additional reagents to activate (iron and acid or chelating agent)
- The hydroxyl radical has a short lifespan, allowing only a limited time for contact with the contaminant and presents a challenge in effective distribution of the oxidant
- Aquifers with high carbonate content can lead to higher consumption of the oxidant
- If significant heat is generated in the subsurface, it may be necessary to use materials other than polyvinyl chloride to construct injection and monitoring wells
- Rapid reaction kinetics and the exothermic nature of the reaction necessitate that the iron and hydrogen peroxide not be mixed together above ground. Additional equipment may be required to handle, store, and introduce both reagents into the aquifer
- CHP offers advantages for sites contaminated with NAPLs. The exothermic nature of the reaction of hydrogen peroxide with

organic matter raises the temperature of the aquifer. The elevated aquifer temperature promotes desorption and solubilization of sorbed NAPL into the aqueous phase, which is where the oxidation reaction occurs. Increased aquifer temperature is most prominent when a high concentration of hydrogen peroxide is used. Hence, it is not uncommon to use concentrations of peroxide up to about 12% at sites that contain NAPL; however, additional health and safety precautions must be employed

- CHP reacts more rapidly with the more toxic aromatic fraction (e.g., benzene and naphthalene) than the aliphatic fraction of petroleum hydrocarbons. Hence, treatments can be implemented that render petroleum hydrocarbons less toxic
- CHP is often employed using a phased approach with other oxidants, where it is used for an initial application to reduce high starting concentrations and NAPL mass, while a different oxidant is used as for additional applications as a polishing step that is more persistent and lower cost

Resources

EPA. A Citizen's Guide to Chemical Oxidation (2001)

This fact sheet provides a brief overview of chemical oxidation and its benefits.

EPA. Engineering Issue: In-situ Chemical Oxidation (2006)

The engineering issue summarizes the fundamentals of ISCO remediation technology based on peer reviewed literature, EPA reports, etc.

ESTCP. In Situ Chemical Oxidation for Remediation of Contaminated Groundwater: Summary Proceedings of an ISCO Technology Practices Workshop Project ER 0623 (2008)

This project provides several documents that help site managers – site specific engineering and application, case histories and database, supplemental information and tools and frequently asked questions guide.

ESTCP. In Situ Chemical Oxidation for Groundwater Remediation (2011) Environmental Remediation Technology

This book presents detailed design guidance and scientific basis for the application of ISCO.

ITRC. Technical and Regulatory Guidance for In Situ Chemical Oxidation of Contaminated Soil and Groundwater. Second Edition (2005)

The guidance document outlines chemical oxidation technologies and their delivery techniques – hydrogen peroxide, potassium and sodium permanganate, sodium persulfate and ozone.

NAVFAC. In Situ Chemical Oxidation Fact Sheet

This fact sheet provides an overview of the ISCO technology and lessons learned during its implementation.

NAVFAC. [In Situ Chemical Oxidation \(ISCO\) Web Tool](#)

This tool presents the current state of ISCO technology, a discussion of how each type of ISCO chemical works, and case studies that showcase their application. This technology involves the subsurface delivery of a chemical oxidant to destroy organic contaminants, reducing potential risks to public health and the environment.

NAVFAC. Cost and Performance Report for Persulfate Treatability Studies (2010)

The report presents five persulfate application projects at four Navy sites and one Marine Corps site. It provides lessons learned and other performance-related information under different site conditions.

NAVFAC. RITS on In Situ Chemical Oxidation (2010)

This presentation provides an introduction to ISCO, its design, implementation and monitoring practices. In addition, it includes a discussion on case studies.

NAVFAC. Best Practices for the Injection and Distribution of Amendments (2013)

This guidance document provides a variety of best practices to effectively distribute amendments for technologies including ISCO, in situ enhanced bioremediation, and in situ chemical reduction.

NAVFAC. Design Consideration for In Situ Chemical Oxidation (2015)

Provides a summary of best practices for ISCO design, tips for appropriate quality assurance and quality control (QA/QC) measures.

Strategic Environmental Research and Development Program (SERDP)/Environmental Security Technology Certification Program (ESTCP). In Situ Chemical Oxidation for Groundwater Remediation (2011)

R.L. Siegrist, M. Crimi, and T.J. Simpkin (eds.). Springer, New York. SERDP ESTCP Environmental Remediation Technology, Vol. 3, ISBN 978-1-4419-7825-7, 678 pp, 2011

Provides principals and best practice for design, application, and monitoring of in situ chemical oxidation remedies.

SERDP. Using Electrical Resistivity Imaging to Evaluate Permanganate Performance During In Situ Treatment of an RDX-Contaminated Aquifer ER-200635 (2009)

The project demonstrates the use of electrical resistivity imaging (ERI) to monitor and facilitate an ISCO demonstration designed to treat RDX with permanganate at the Nebraska Ordnance Plant.

SERDP. Improved Understanding of In Situ Chemical Oxidation (ISCO) ER-1289 (2010)

This project provides improved understanding of ISCO applicability and optimized deployment conditions through two separate bench-scale efforts.

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1. Ozone also is used at some sites. However, ozone is introduced as a gas, which requires a different design and method of introduction and associated challenges. Hence, it is not covered in this technology profile. [↩](#)
 2. Ozone also is used at some sites. However, ozone is introduced as a gas, which requires a different design and method of introduction and associated challenges. Hence, it is not covered in this technology profile. [↩](#)
 3. Effective for naphthalene, phenanthrene, and pyrene [↩](#)
 4. Effective for naphthalene, phenanthrene, and pyrene [↩](#)
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