

# The Application of In Situ Chemical Oxidation (ISCO) in Fractured Bedrock using Geophysical Aided Design

Presented by Susanne Borchert  
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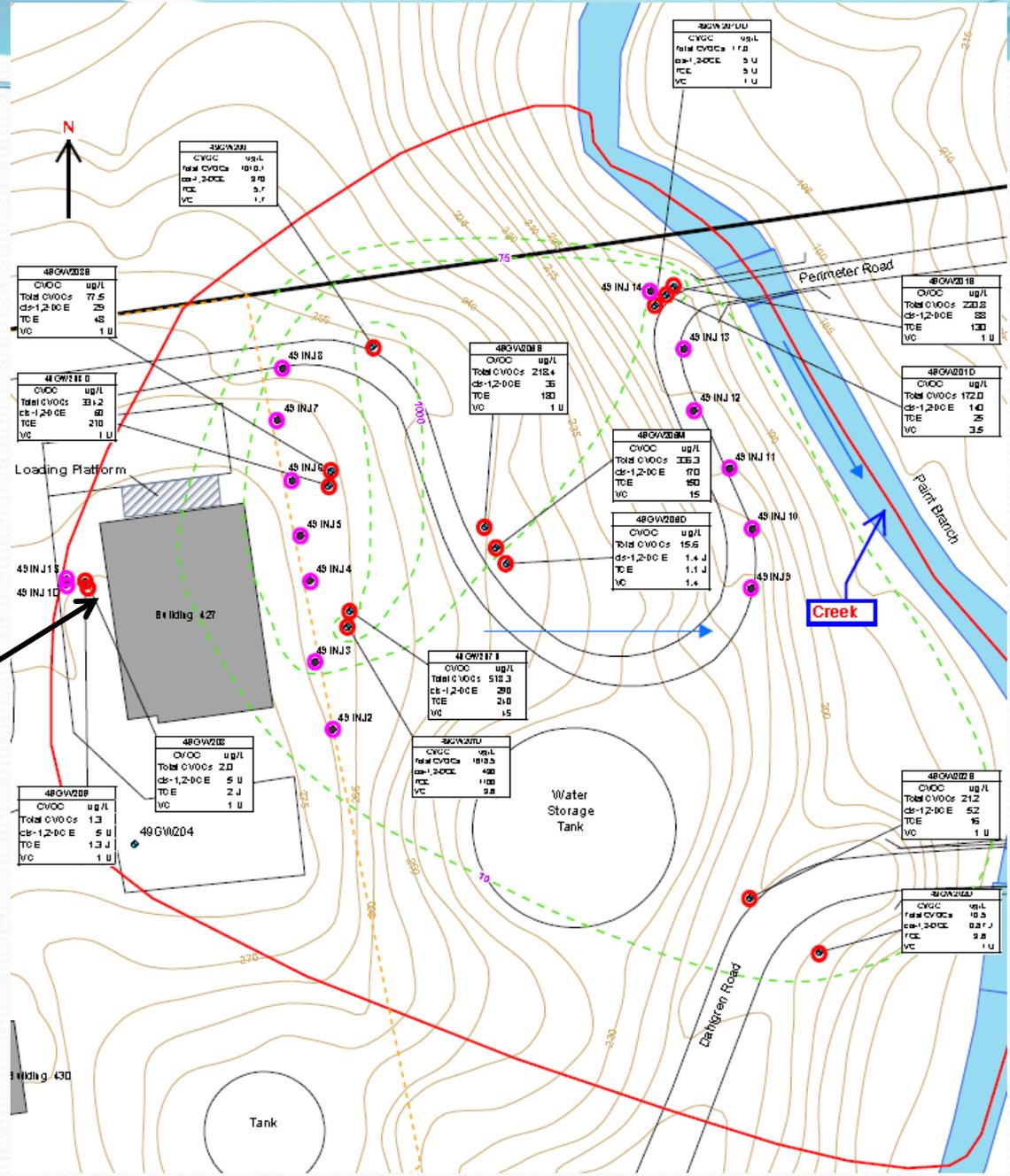
# Presentation Overview

- Present case studies highlighting the **bedrock characterization elements used in ISCO designs**
- Show how results were used to
  - a) determine oxidant quantity (dosage)
  - b) assess ISCO delivery approach
- Discuss lessons learned

# Background of Maryland Site

- Piedmont bedrock– garnet-bearing schist and quartzite to 150 feet below ground surface (ft bgs)
- Contaminants ( $\mu\text{g/L}$ ): TCE =4,400, cis-DCE =1,100, VC = 81
- Groundwater table near source is in bedrock (56 ft bgs), extends into saprolite in downgradient direction (8 ft bgs) near creek to east
- $i_h = 0.1$  to  $0.4$  ft/ft; complex  $i_v$  - mostly downward near source, slightly upward by creek
- $k$  in bedrock  $0.36$  ft/day; in saprolite  $0.14$  to  $1.01$  ft/day

# Plan View

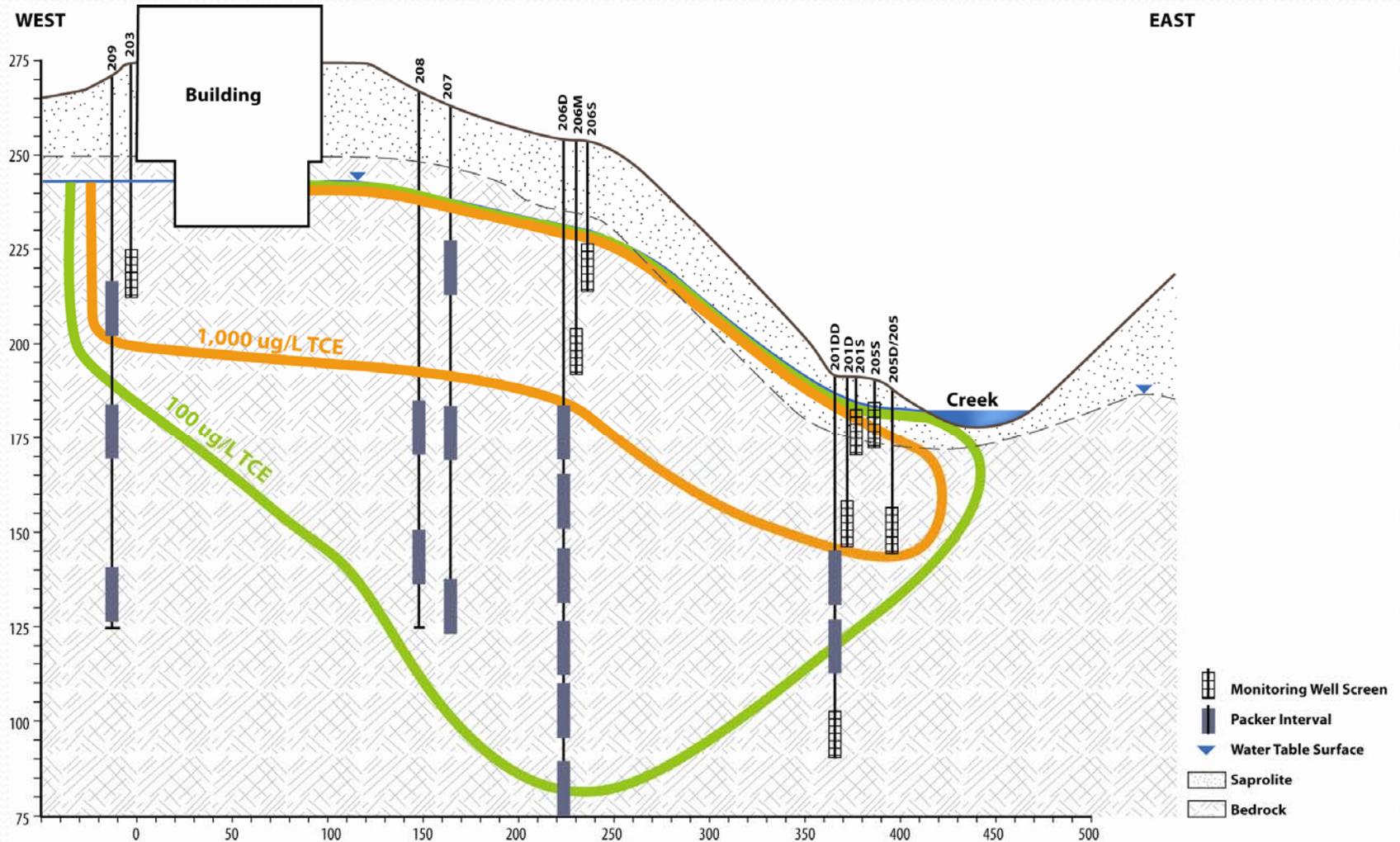


Source  
(Dry Well)

red=MWs

lilac=IWs

# Cross-Section



# Field Tests Conducted in Bedrock

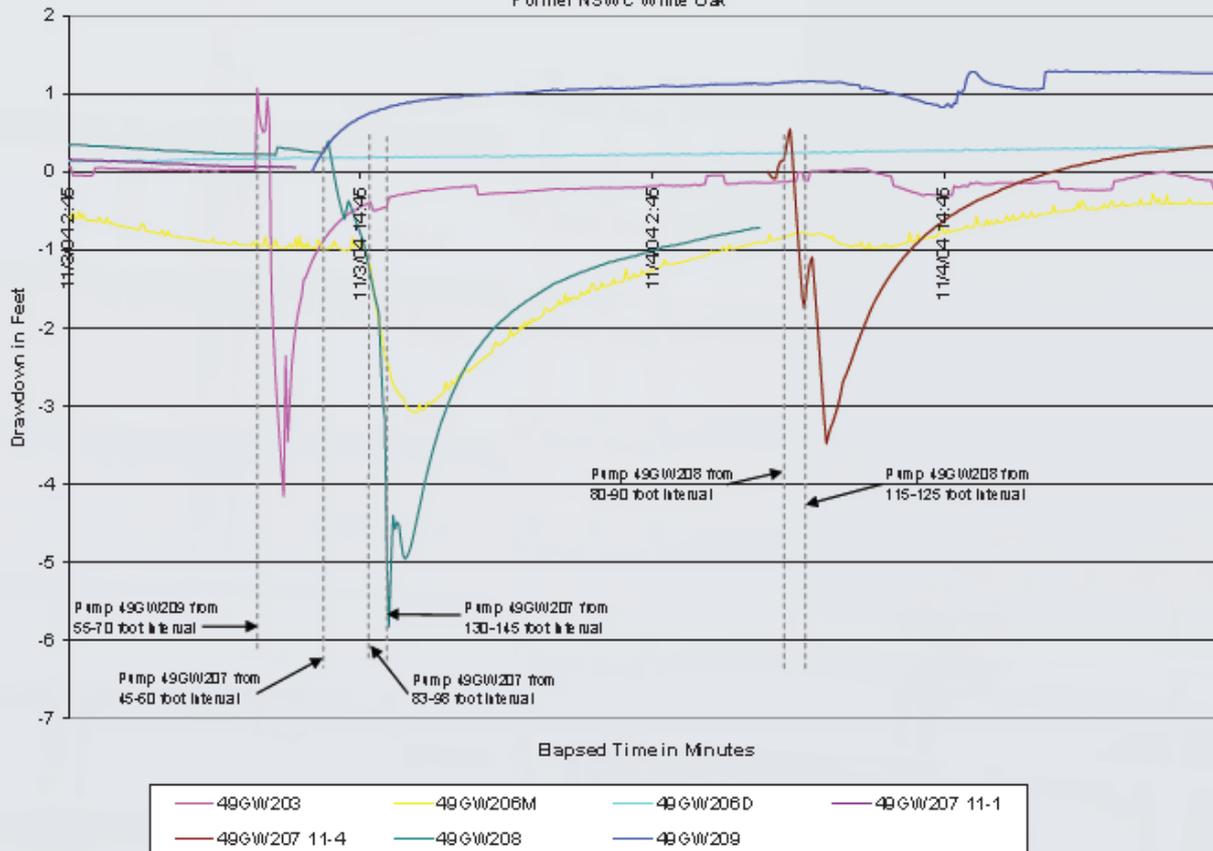
- Wells sampled for VOCs including using isolated profiling with packers
- Hydraulic connectivity testing in open boreholes
- Borehole caliper, optical televiewer, heat-pulse flow meter and fluid resistivity
  - Borehole fracture aperture were analyzed according to the **Paillet ranking method** due to their importance for the ISCO design – as they **determine the quantity and distribution of groundwater in the bedrock matrix**

Well ID	Total # of Fractures	Paillet Ranking				
		1	2	3	4	5
GW207	13	12	1	-	-	-
GW208	5	5	-	-	-	-
GW209	7	7	-	-	-	-

(Note – Total oxidant demand [TOD] tests not conducted on bedrock sample/core. Bedrock oxidant demand is assumed to be negligible since contact in fractures is less than in unconsolidated matrix)

# Hydraulic Connectivity Test Result

Packer Test Transducer Data  
Site 49 Pre-Design Investigation  
Former NSWC White Oak



Boreholes pairs showing hydraulic connection:

- 209-203
- 206-207
- 207-208

# ISCO Oxidant Demand Design

## Initial ISCO design (inject and drift approach):

- Groundwater volume requiring treatment
  - Average width of fracture openings per linear borehole foot
  - Areal extent to treat
- Only used stoichiometric demand of VOCs for dosage
  - assume oxidant demand of bedrock is negligible
  - safety factor of 3 to increase longevity/persistence of permanganate
- 120 to 480 gallons of 5% by weight Na-permanganate per injection well;
- 2,480 total gallons oxidant solution and 1,360 pounds permanganate
  - Individualized per IW depending on inches of open fractures and treatment area (pore volume)

## Optimization after installed and characterized 15 injection boreholes:

- 40 to 125 gal of 8% by weight Na-permanganate , with 70 to 200 gallons chase water
  - 1,365 total gallons oxidant plus 2,220 gallons chase water and 1,100 pounds permanganate (average 3 gallons per minute injection)
- (reduced permanganate solution to <60% of fractured bedrock pore volume)

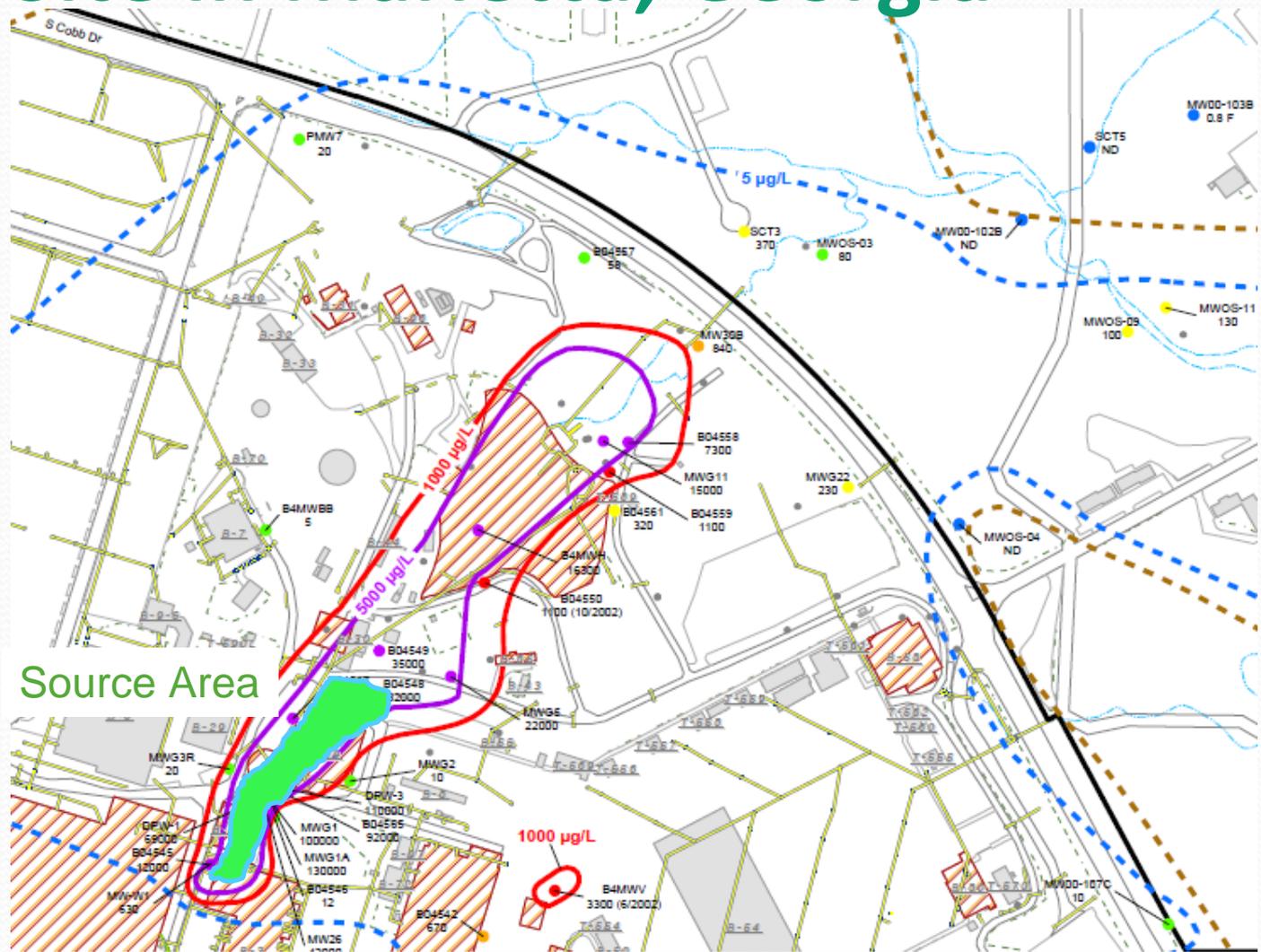
# Effectiveness Overview

- Permanganate longevity less than 1 year except one well
- Overall areal extent of plume decreased
- TCE decreased initially, rebounded slightly after second year
- cis-DCE and VC decreased slightly
- Configuration of VOC concentration contours showed spotty reductions

Lesson learned: Would be beneficial to test connectivity of injection wells to monitoring wells prior to application

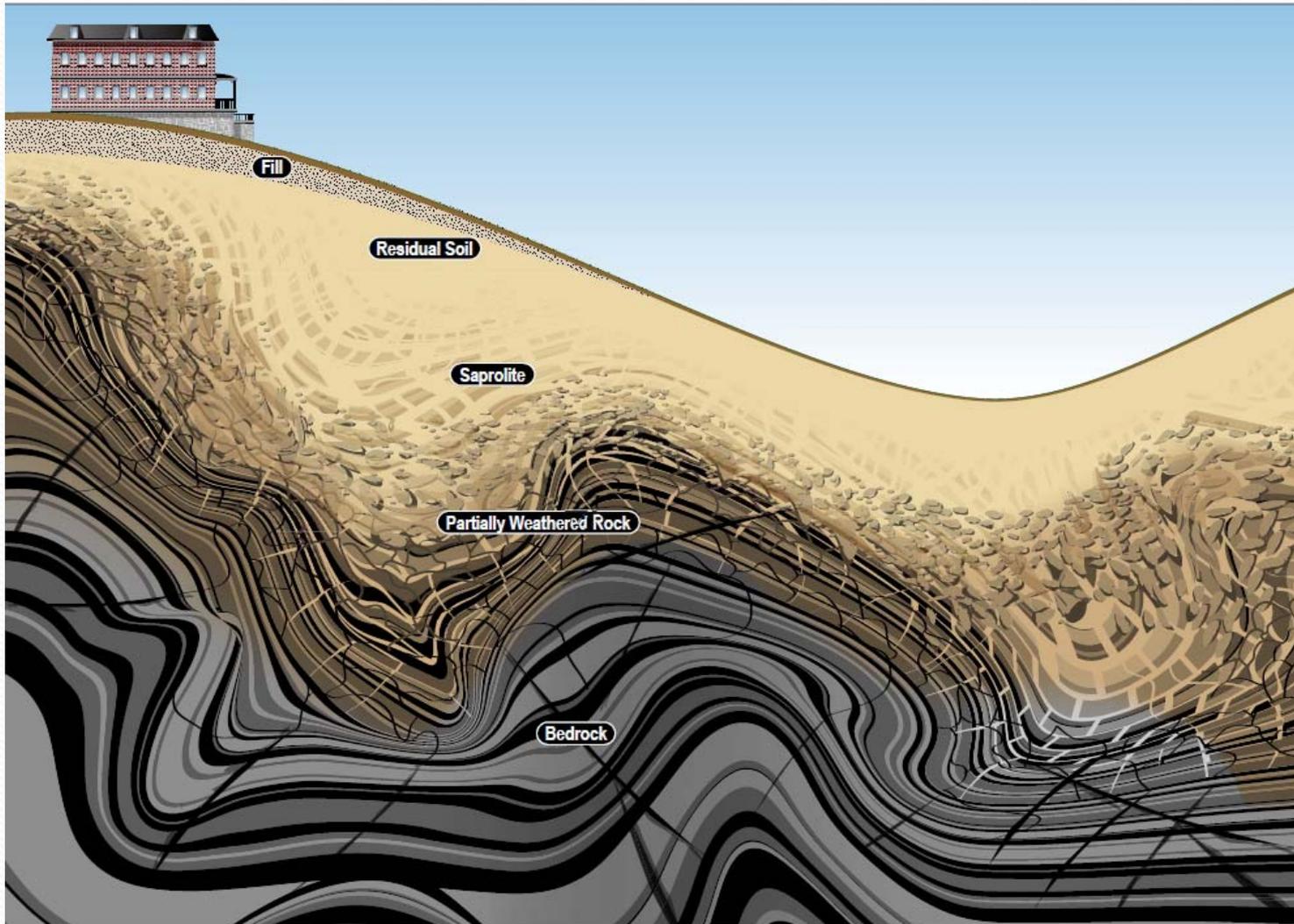


# Site in Marietta, Georgia



Source Area

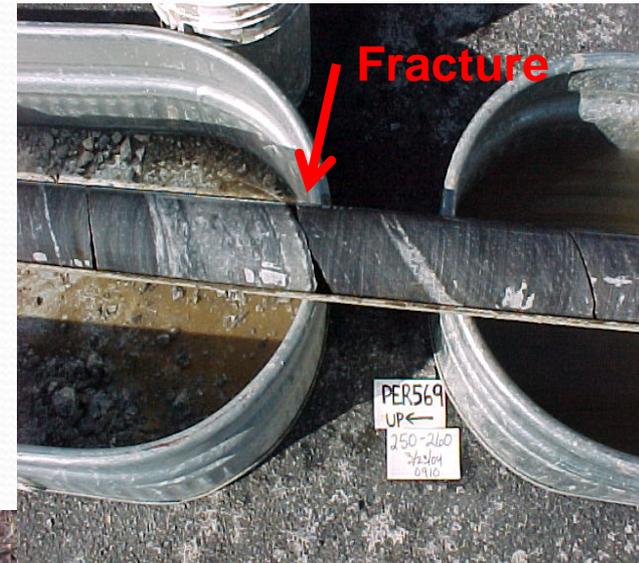
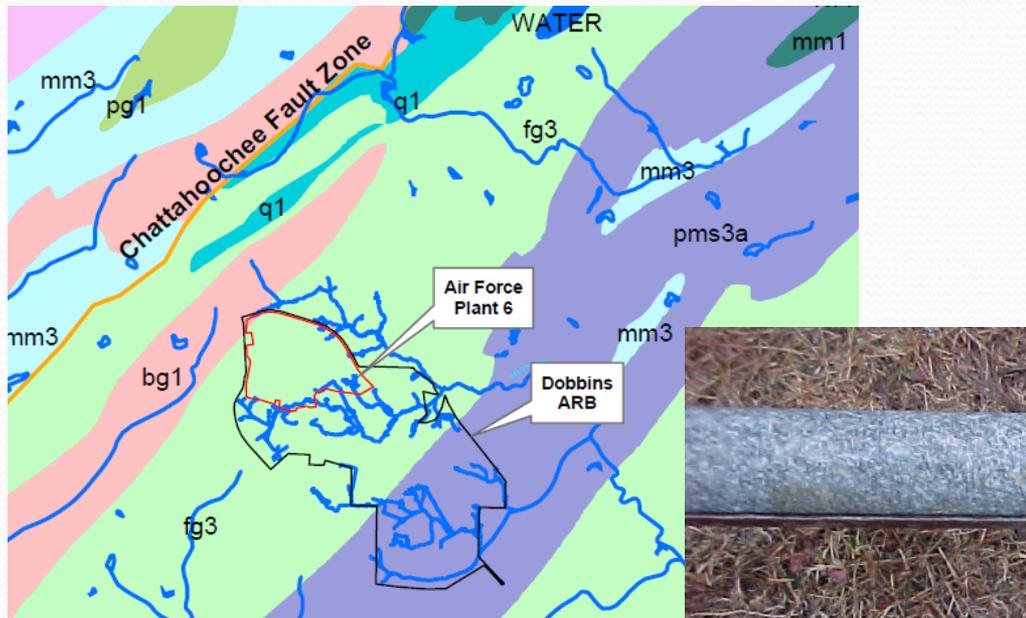
# Lithology Model



# Field Characterization Methods

- Test borings
  - Soil and rock cores (field descriptions)
  - Field and lab tests (Sudan IV dye, FLUTe™ liners, chemical analyses, rock quality designation – RQD)
- Wells
  - Water level measurements to predict horizontal and vertical flow
  - Water samples to define horizontal and vertical plume extent
  - Borehole logs (caliper, acoustic and video televiewer, heat pulse flow meter, electrical resistivity, gamma)
  - Aquifer tests

# Bedrock is biotite gneiss, micaschist, and granite



# Borehole Logging Results

- Bedrock had no water bearing fractures below 250 ft bgs
- Nearly all water conducting fractures parallel to rock fabric or foliation
  - One water-producing fracture per 100 ft (low count!)
  - Poor vertical interconnection of fractures (pulse heat flow meter, substantial heads between fractures in same borehole)
- Fracture porosity <0.01% of bedrock

Conclusion: although high TCE concentrations in fractures (>100,000  $\mu\text{g/L}$  TCE) migrating in few, and horizontally isolated fractures - not much TCE mass in bedrock (probably <5%)

# ISCO Design and Results

**Strategy: address zones with highest TCE mass, use technologies that will show results in <3 years**

- ISCO in PWR within “source area”, to also treat TCE in fractured bedrock
- PWR and bedrock assumed to have no oxidant demand
- Used K-permanganate (more cost effective) and mixed in 4% solution
- Pilot test showed anisotropy in injection radius; estimated volume of PWR
- Injected about 16,000 gallons in 32 injection wells (one pore volume)

**Implementation started in late 2008.  
Results to date:**

- Eliminated 100,000  $\mu\text{g/L}$  plume in “source area” bedrock
- PWR 10,000  $\mu\text{g/L}$  plume reduced by 68%
- PWR 100,000  $\mu\text{g/L}$  plume reduced by 80%



ISCO Mix Area

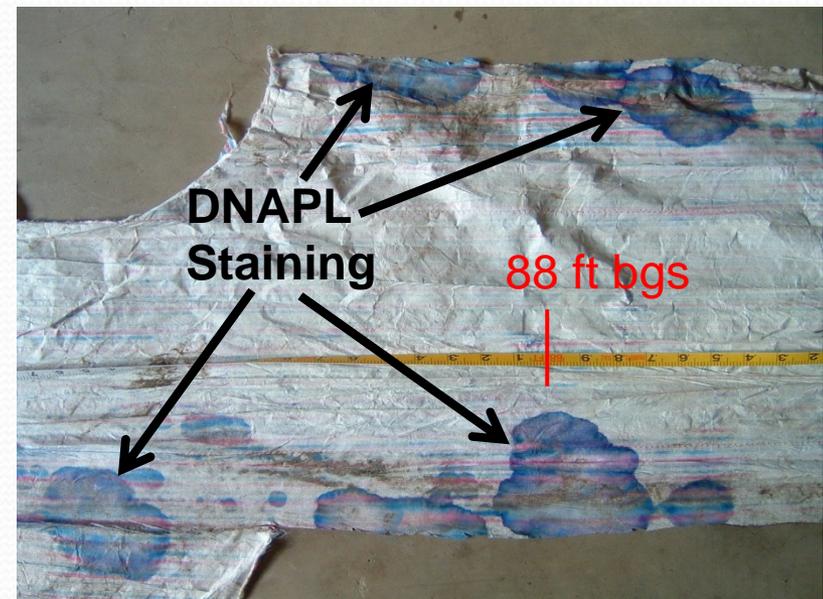
# Background of West Virginia Site

- Site was research and production facility for solid propellants
- Approximately 1,000 pounds per month of TCE were disposed in three unlined pits between 1970 and 1978
- Fill and alluvium underlain by fractured shale bedrock
- Natural groundwater flow is toward NE (to North Branch Potomac River)
- Current groundwater extraction system captures contaminated groundwater before entering river
- Pilot study performed in solvent disposal pit area of Site 1 to evaluate ISCO's ability to reduce VOC mass in fractured bedrock aquifer



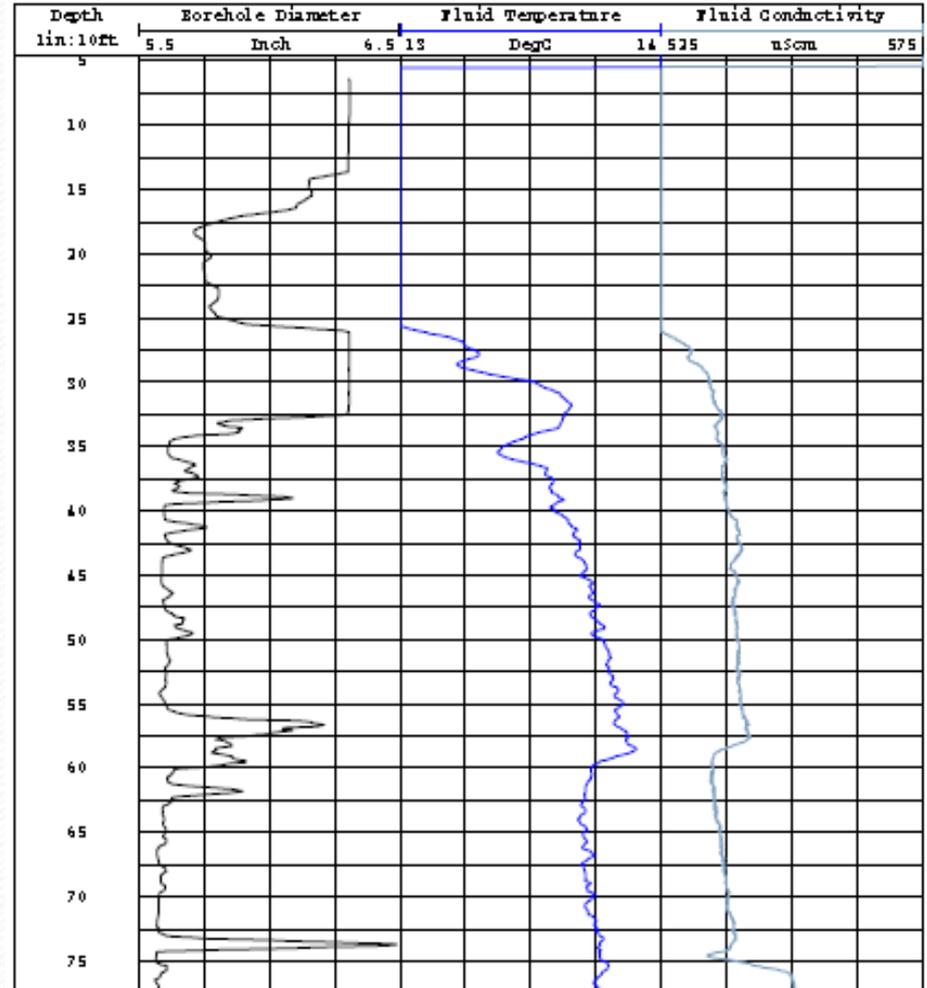
# Site Characterization

- Limited down-hole geophysics on monitoring and injection wells (caliper log, fluid temperature log, fluid conductivity log)
- FLUTE™ liners to verify the presence and location of DNAPL in fractures
- Collect and analyze borehole groundwater samples using low flow techniques (vs. packers)



# Geophysical Results

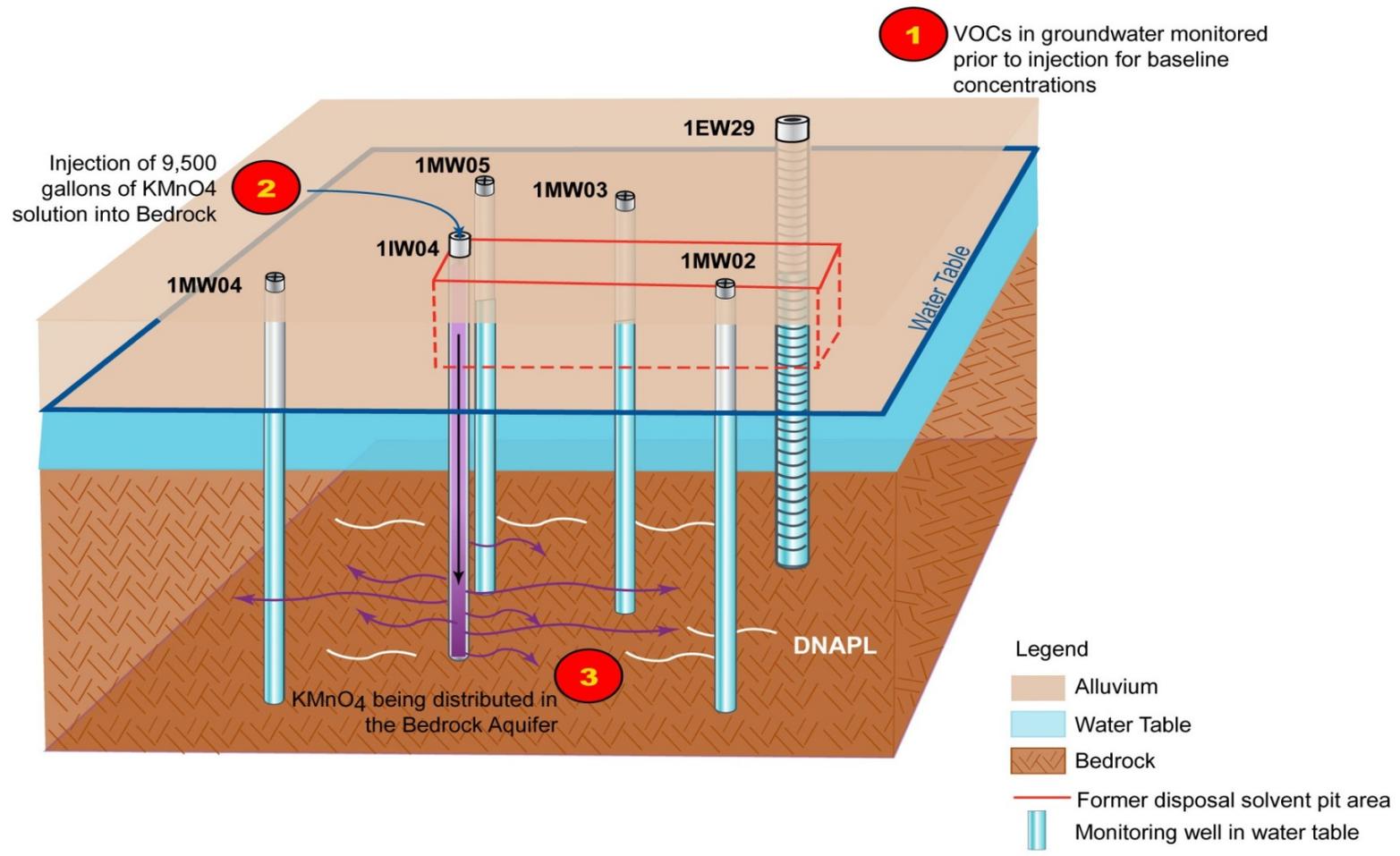
- Caliper log
- Fluid temperature log
- Fluid conductivity log
  
- Shale has extensive horizontal fractures that are also pretty well connected vertically; relatively high bedrock porosity



# ISCO Pilot Study Design

- Goal: TCE mass reduction, flux reduction downgradient
- Oxidant selected: potassium permanganate ( $\text{KMnO}_4$ )
  - Wanted to avoid oxidants that need catalyst, mixing in situ
- 3,200 lbs of K-permanganate mixed with water, 9,500 gallons 3% by weight solution
- 6,300 gal gravity fed at 9 to 12 gpm, 3,200 gallons injected with low pressure at 12 to 14 gpm
  - Observed almost immediate impact on surrounding wells
  - Displacement not critical issue during pilot study: small treatment area, high porosity, groundwater extraction system

# Pilot Study Layout



NOTE: Wells installed approximately 90' below ground surface.

# Pilot Study Results

- Downgradient extraction well had K-permanganate shortly after injection; was turned off for pilot study duration

<b><u>Sampling Event</u></b>	<b><u>Maximum TCE</u></b>	<b><u>Average TCE</u></b>
<b>Baseline</b>	<b>110,000</b>	<b>28,500</b>
<b>3 Week</b>	<b>100</b>	<b>12</b>
<b>6 Week</b>	<b>190</b>	<b>45</b>
<b>3 Month</b>	<b>14,000</b>	<b>4,100</b>
<b>5 Month</b>	<b>13,000</b>	<b>4,500</b>

# Pilot Study Conclusions

- Total VOCs decreased 84% in the bedrock aquifer
- Based on vertical ORP trends in boreholes, permanganate evenly distributed
- Rebound observed, likely caused by
  - Migration of alluvium and upgradient dissolved phase VOCs
  - Continued dissolution of DNAPL
- Higher dose permanganate may persist longer and oxidize more mass before rebound occurs
- ISCO may be more effective if the extraction system shutdown to increase permanganate residence time



# Lessons Learned

- Characterization tests that end up **most** useful at any given site are unpredictable, need multiple lines of evidence to shape conceptual site model for ISCO design and delivery
  - Televiewer and hydraulic connectivity tests in MD
  - Caliper, televiewer, and heat pulse flow meter in GA
  - FLUTE™ liners, caliper, fluid temperature and conductivity in WV
- To mitigate plume displacement by oxidant solution, use small injection volumes (fraction of estimated pore volume).
  - Don't underestimate transport distance of low volume of injectant in fractures/lineaments – monitor potential surfacing
- During ISCO injection in open borehole extending beyond treatment zone, consider placing packer below lowest impacted, water-bearing fracture
  - Enhances use of oxidant to destroy contaminants in open fractures